

Development of CATIA_2_GEANT Interface for Simulation of High Energy Physics Experiments



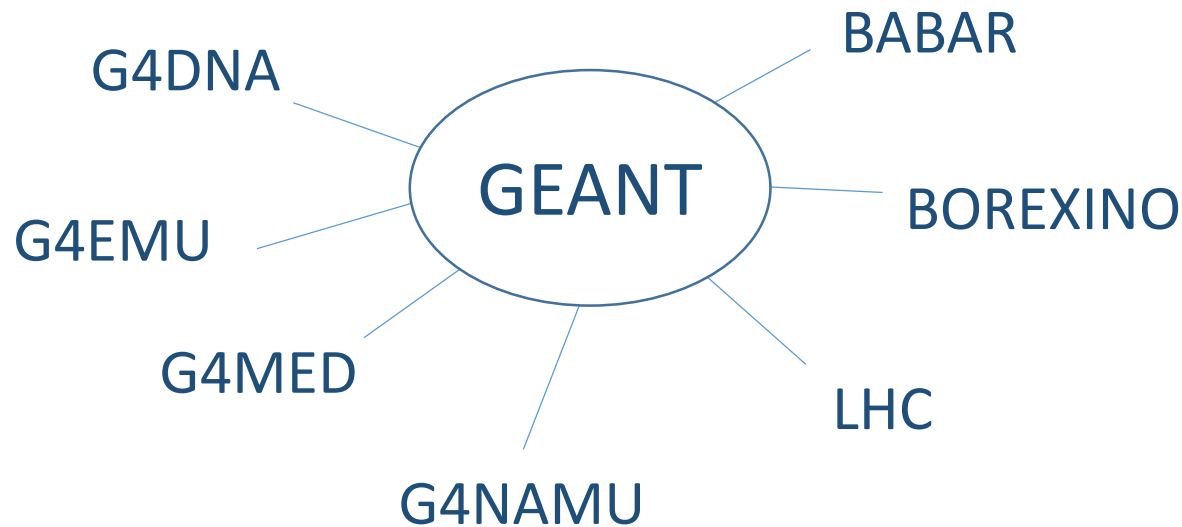
SHARMAZANASHVILI Alexander
ATLAS Collaboration



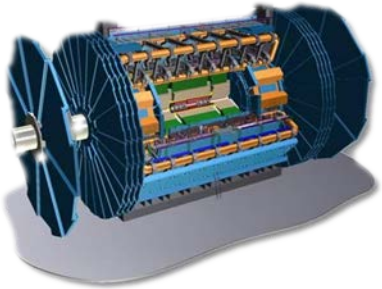
TSUTSKIRIDZE Nikoloz
Georgian Technical University



- GEANT is a platform for simulation of facilities and physical events by modelling of the passage of particles through the matter
- GEANT implementing in High Energy, nuclear and Accelerator physics as well for studies in medical and in space science

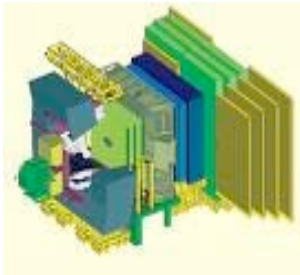


LHC Machine at CERN



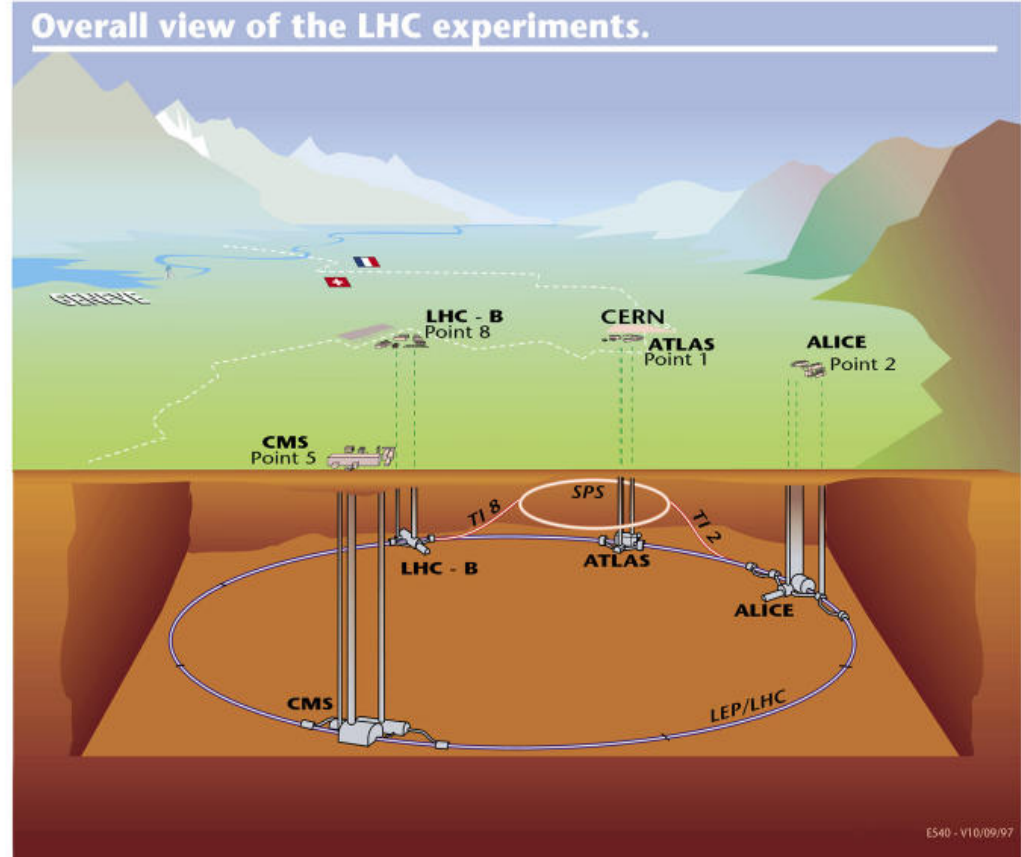
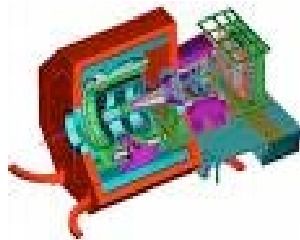
ATLAS Detector length
~40 m, height ~22 m,
weight ~7'000 tonnes

CMS Detector length ~22 m,
height ~15 m, weight
~14'000 tonnes



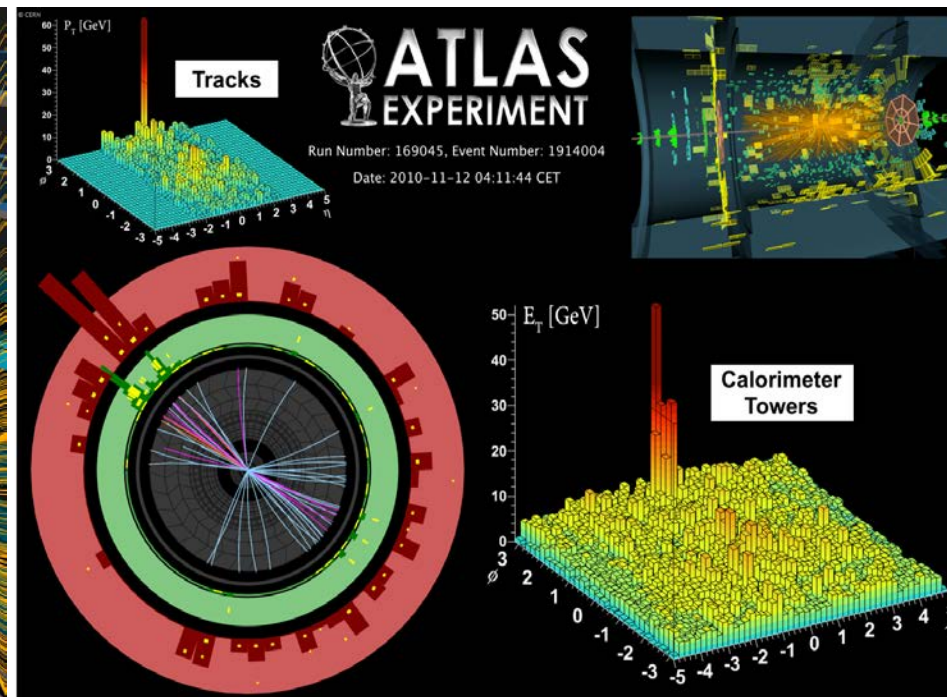
ALICE Detector

LHCb Detector

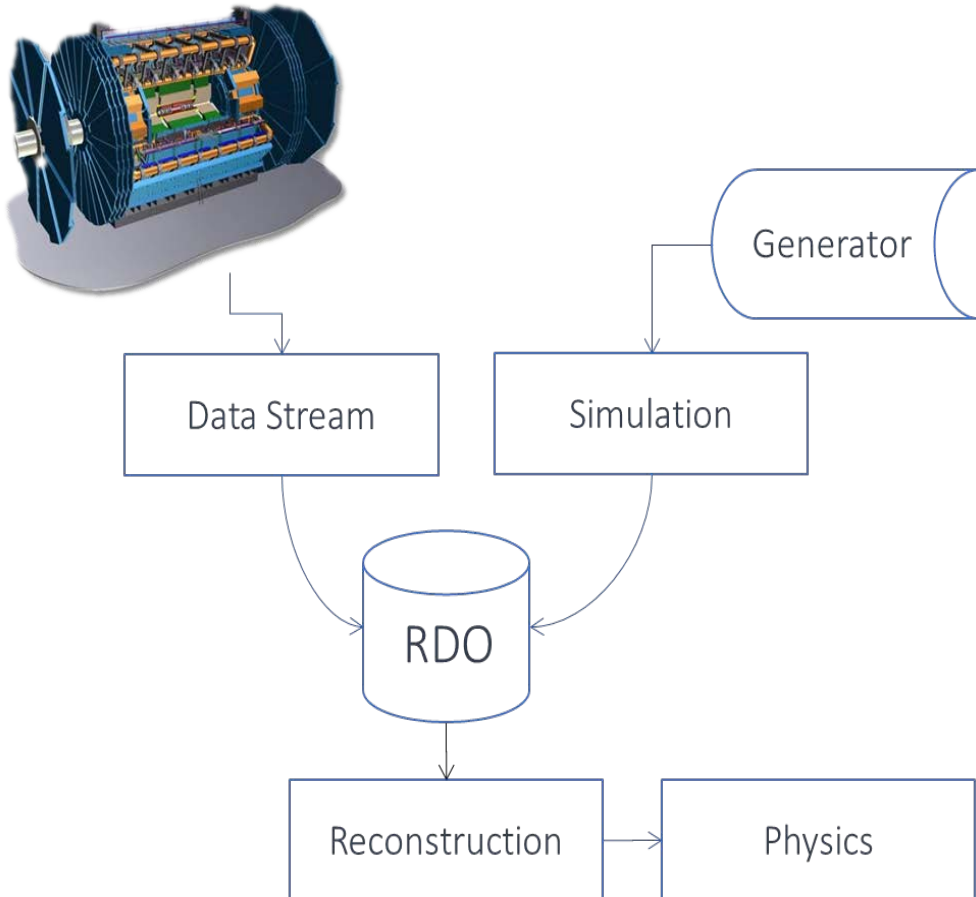


ATLAS Experiment

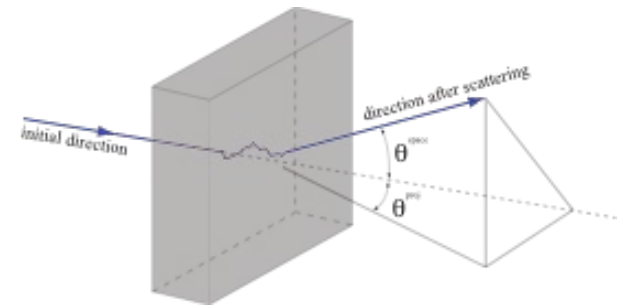
- ATLAS implements simulation for deep and wide range investigation of physics experiments by generating artificial events from the event generator in a format which is identical to the output of the detector data acquisition system



ATLAS Experiment



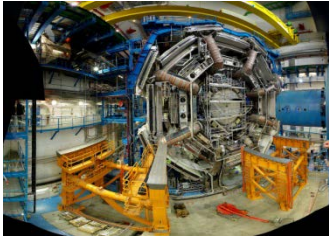
- The passage of a particle through matter



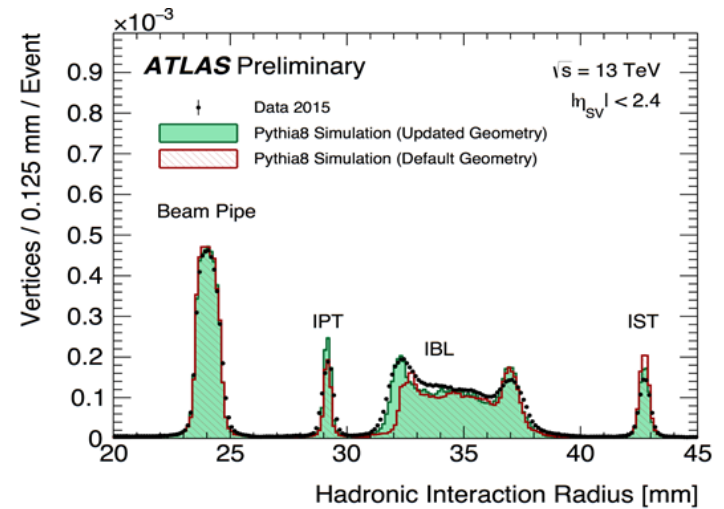
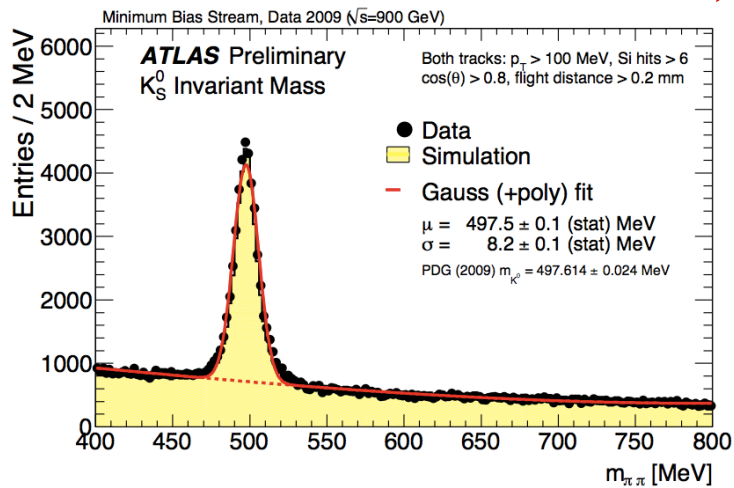
$$\langle Q_{\text{proj}}^2 \rangle = \frac{(21 \text{ MeV})^2 (m^2 + p^2)}{2p^4 \beta^2} \frac{x}{x_0} \left(1 + 0.038 \log \frac{x}{x_0} \right)^2 \frac{\langle Q_{\text{space}}^2 \rangle}{2}$$

Problem of Data Discrepancy

Reality



Monte Carlo Simulation

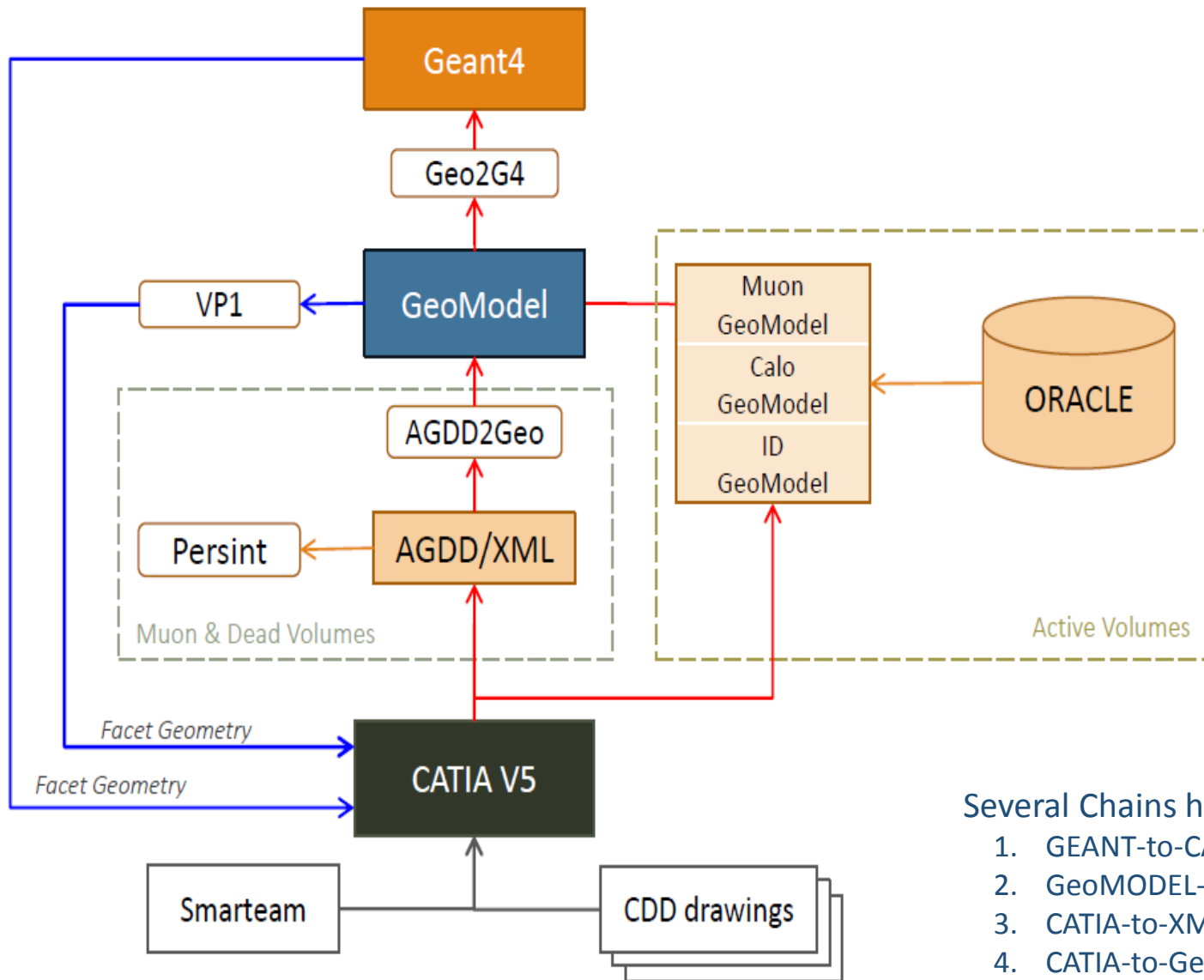


Analyze & Compare

Research Hypothesis

- Several reasons can cause discrepancies between Data and Monte-Carlo. Several investigations show that they are coming by the reason of geometry descriptions in simulation
- It is possible to predict 2 hypothesis why faults are exist in geometry descriptions:
 - Hypothesis #01: Inaccuracies added by geometry transactions of simulation software infrastructure
 - Hypothesis #02: Inaccuracies added by difference of as-built geometry descriptions with geometry descriptions of simulation

Geometry Simulation Loop



Several Chains have been developed:

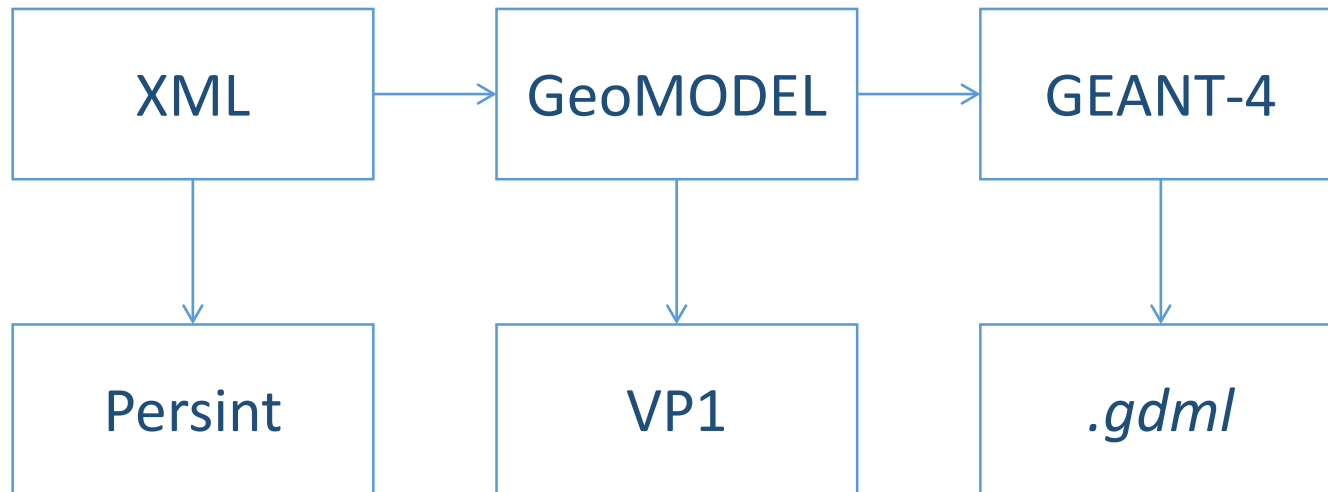
1. GEANT-to-CATIA
2. GeoMODEL-to-CATIA
3. CATIA-to-XML
4. CATIA-to-GeoMODEL

Checking Hypothesis 01:

Investigation of Simulation Infrastructure

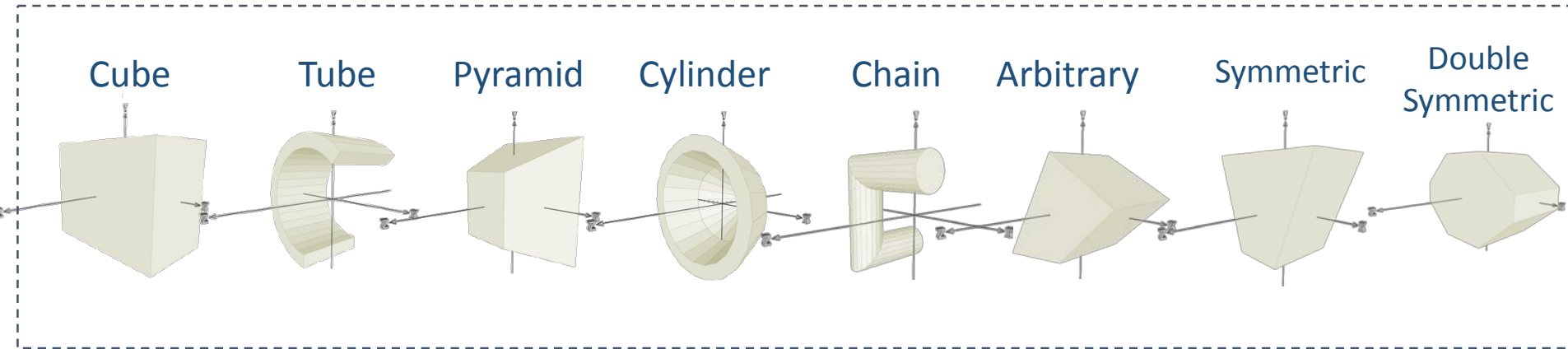
Investigation of Simulation Infrastructure

- ATLAS simulation infrastructure use 3 platforms for description of detector geometry: GEANT, GeoMODEL and XML.
- Geometry descriptions on GEANT and GeoMODEL are generating at run-time during the simulation session, while XML descriptions stored in database



XML Platform

- Standard Primitives and Polygon Methods



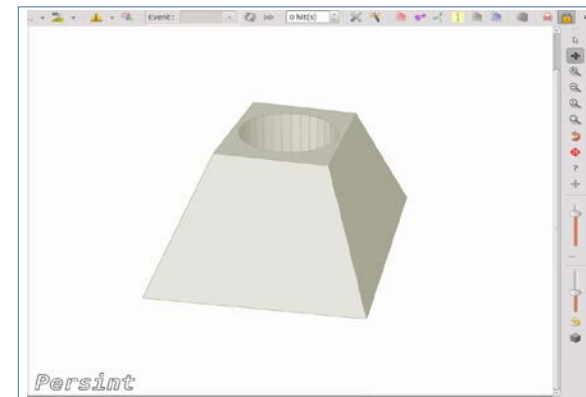
- Transactions: Move, Rotate
- Boolean Operations: Subtraction, Union, Intersection

Code Example for *Pyramid* with cut

```
<trd name="Pyramid" material="Aluminium" Xmp_Ymp_Z="4000.; 2000.; 5000.; 2500.; 3000." />  
<tubs name="Tube" material="Aluminium" Rio_Z="0.; 900.; 5200." nbPhi="32" />  
  
<subtraction name="Pyramid_Test" >  
  <posXYZ volume="Pyramid" X_Y_Z=" 0; 0; 0." rot=" 0.; 0.; 0." />  
  <posXYZ volume="Tube" X_Y_Z=" 0; 0; 0." rot=" 0.; 0.; 0." />  
</subtraction>
```

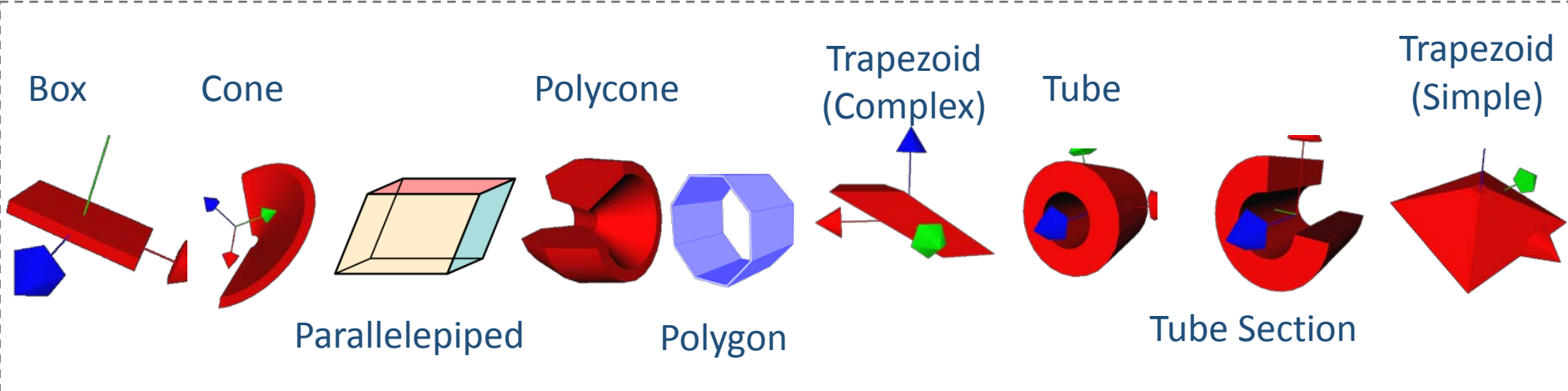


Persint Screenshot



GeoMODEL Platform

- Standard Primitives and Polygon Methods



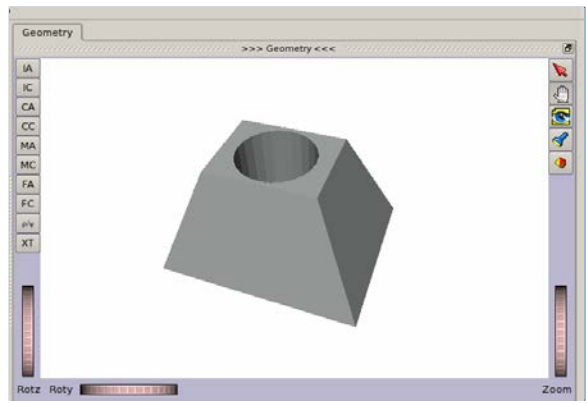
- Transactions: Move, Rotate
- Boolean Operations: Subtraction, Union, Intersection

Code Example for *Pyramid* with cut

```
129
130 GeoTrd * Trapezoir_Pr = new GeoTrd(2000.*CLHEP::mm, 1000.*CLHEP::mm,2500.*CLHEP::mm,
131 1250.*CLHEP::mm, 1500.*CLHEP::mm );
132 GeoTube * Tube = new GeoTube( 0.*CLHEP::mm, 900.*CLHEP::mm, 2600.*CLHEP::mm);
133
134 const GeoShape & ExempleN55_subtr = Trapezoir_Pr->subtract((*Tube));
135
136 GeoLogVol* ExempleN55_Log = new GeoLogVol("ExempleN55",&ExempleN55_subtr,Aluminium);
137 GeoPhysVol* ExempleN55_Log_Phys = new GeoPhysVol(ExempleN55_Log);
138
```

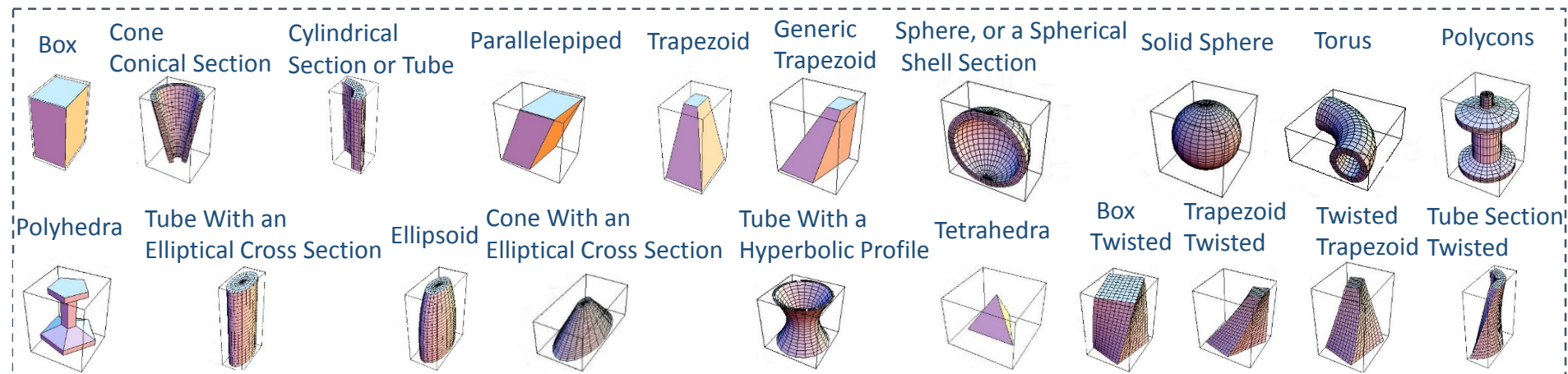


VP1 Screenshot



GEANT-4 Platform

Standard Primitives and Polygon Methods



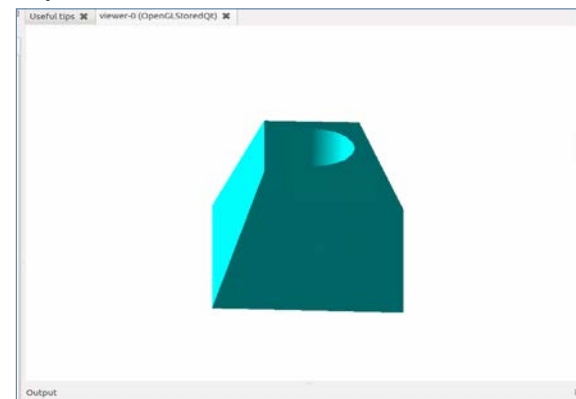
- Transactions: Move, Rotate
- Boolean Operations: Subtraction, Union, Intersection

Code Example for *Pyramid with cut*

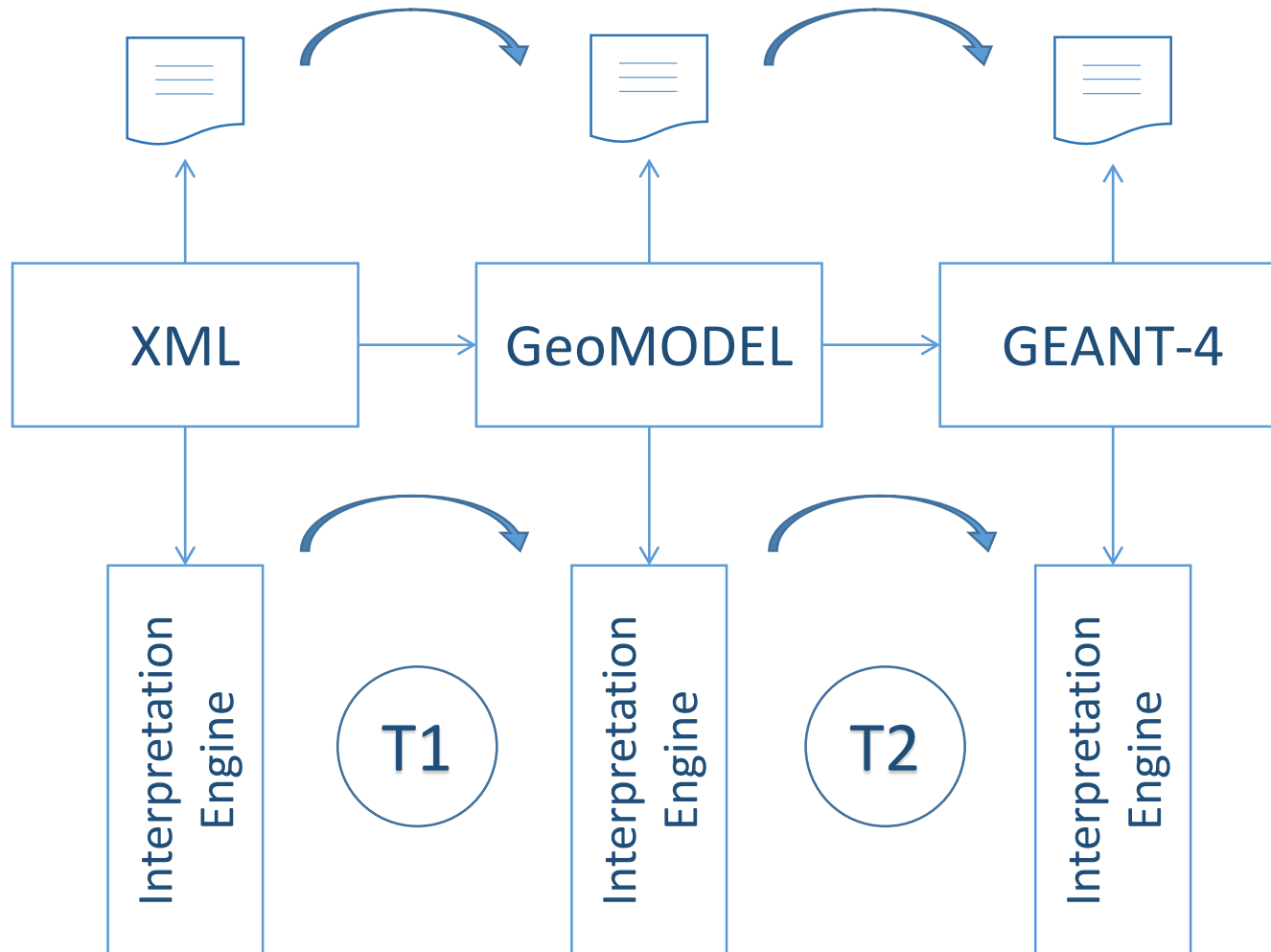
```
150
151
152 G4Tubs* solidShape1 = new G4Tubs("Shape1", 0.*mm, 900.*mm, 5200.*mm, 0.*deg, 360.*deg);
153
154 G4Trd* solidShape2 = new G4Trd("Shape2",
155     2000.*mm, 1000.*mm,
156     2500.*mm, 1250.*mm, 1500.*mm);
157 G4SubtractionSolid* b1minusC12 = new G4SubtractionSolid("Box-Cylinder", solidShape2, solidShape1);
158
159 G4LogicalVolume* b1minusC1 = new G4LogicalVolume(b1minusC12,
160     shape2_mat,
161     "Shape2");
162
163 new G4PVPlacement(0, pos2, b1minusC1, "Shape2", logicEnv, false, 0, checkOverlaps);
164
```



OpenGL Screenshot



Geometry Transformations



Objectives of Analyses

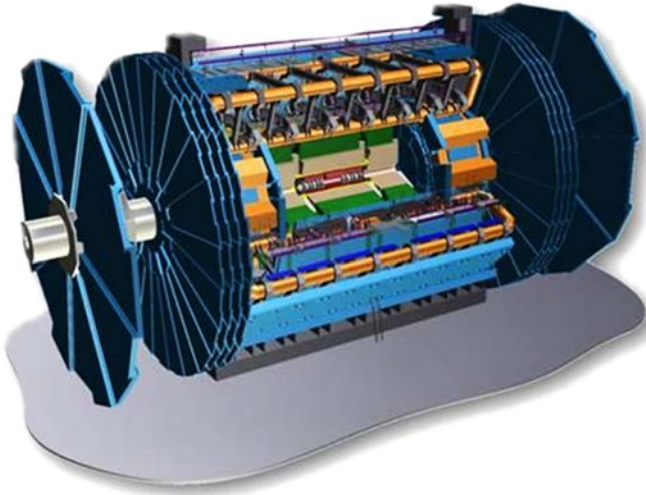
- Investigation quality of T1/T2 geometry Transformations

Methodology of Analyses

1. Categorization of geometry of Detector components
2. Selection Methods for description
3. Test runs of test examples
4. Case study of transactions
5. Systematization and learning of results

Part I. Categorization of Geometry

I. Categorization of Geometry



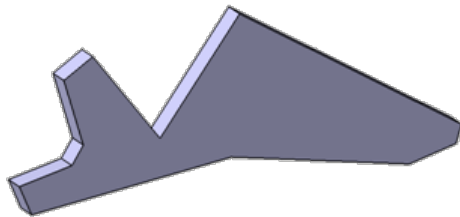
- Total number of Mechanical assemblies > 3'700
- Total number of Mechanical features > 10'000'000
- Disk size of geometry 62Gb

- **Purpose** of categorization is finding groups of detector components similar by geometry and identification of typical group representatives.
- **3 criteria** can be implemented for categorization of detector geometry:
 1. Correspondence of detector components to standard geometry primitives – shapes with vertex; shapes without cuts; both, regular and irregular shapes; both, convex and concave shapes
 2. Grouping components with typical joining's
 3. Grouping components with cuts

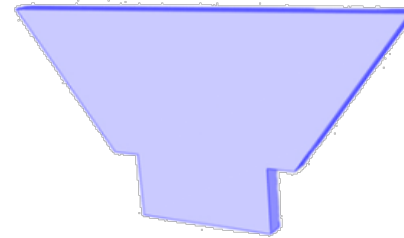
I. Categorization of Geometry

- 22 typical primitives have been separated in 1st class of objects

Dodecagonal Prism

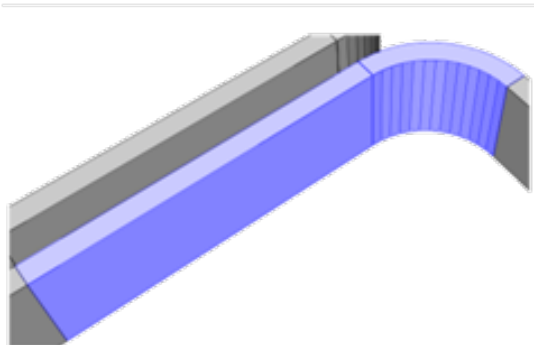


Octagonal Prism

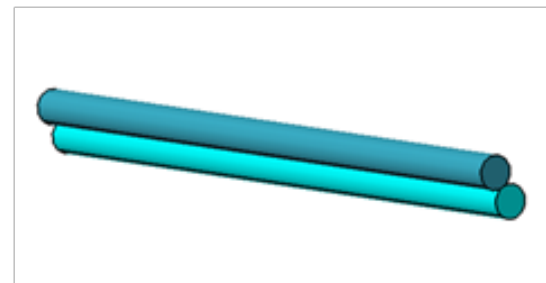


- 29 combined objects with typical joining's have been found for 2nd class

Cube and Tube Joining



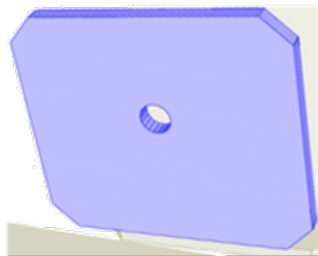
Tubes Joining



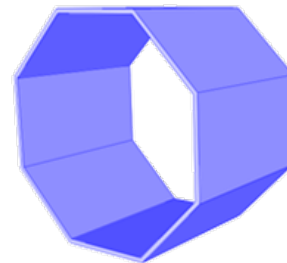
I. Categorization of Geometry

- 3. 33 objects with cuts were separated for 3rd class

Octagonal Prism with cut



Octagonal prism with cut

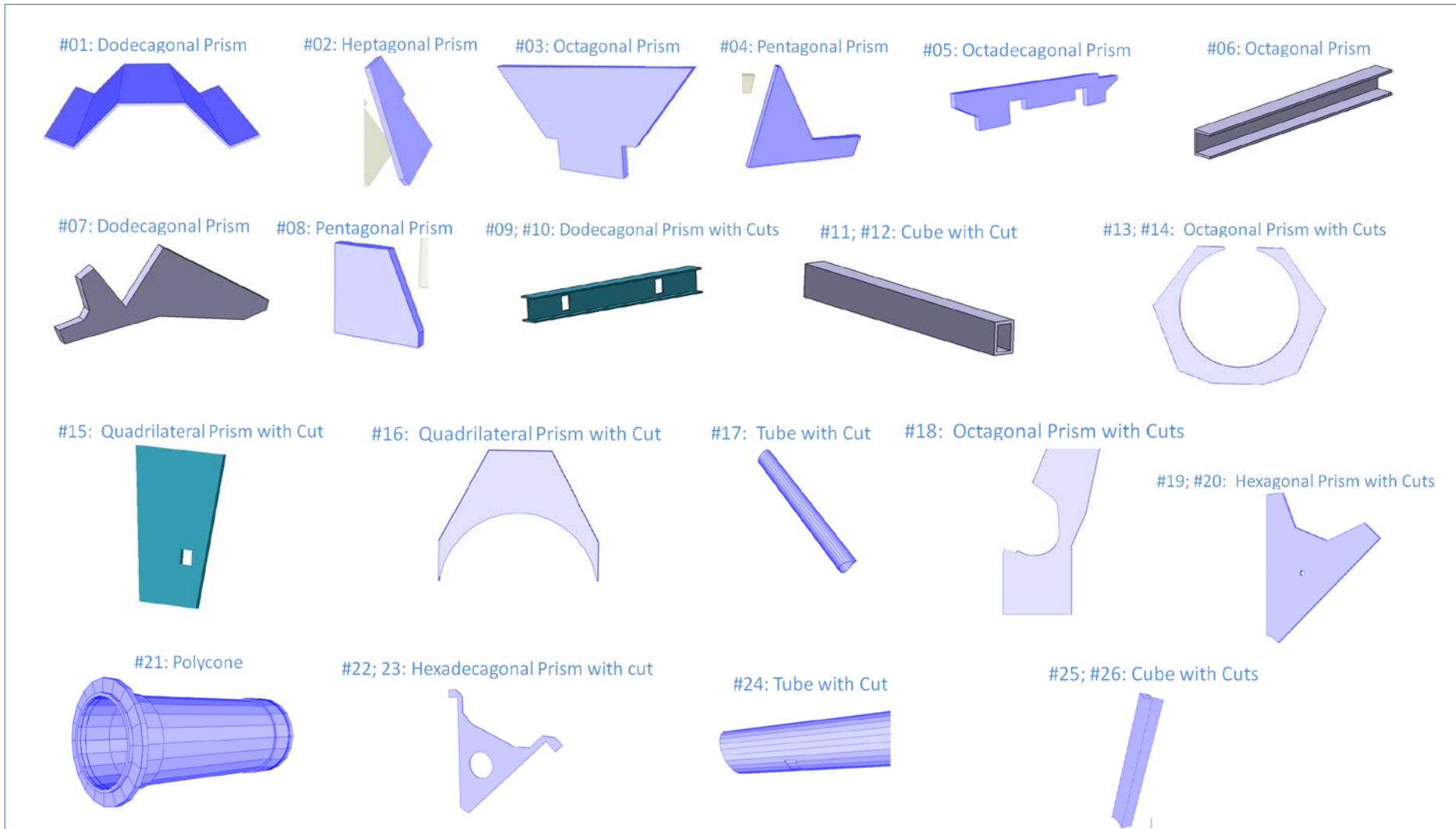


Conclusion: ATLAS detector geometry can be described by 84 typical representors of class of objects

Muon & Dead Volumes	Geometry Primitives	19	Total: 58
	Typical Joining	13	
	Combined Objects	26	
Active Volumes	Geometry Primitives	3	Total: 26
	Typical Joining	16	
	Combined Objects	7	

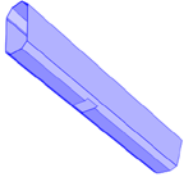
I. Categorization of Geometry

84 typical representors of class of objects



I. Categorization of Geometry

#27; #28: Octagonal Prism with Cuts



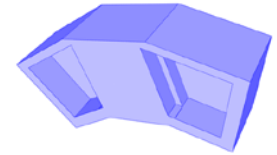
#29: Octadecagonal Prism with Cuts



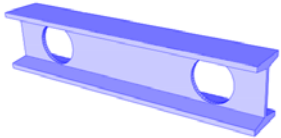
#30; #31: Dodecagonal Prism with Cuts



#32; #33: Octagonal Prism with Cuts



#34; #35: Dodecagonal Prism with Cuts



#36; #37: Octagonal Prism with Cuts



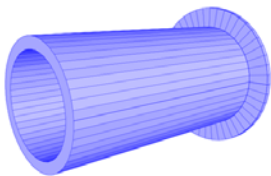
#38; #39: Icositetragonal Prism with Cuts



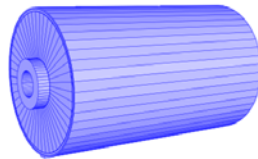
#40; #41: Cube with Cuts



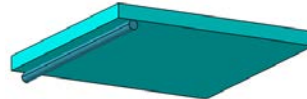
#42: Tubes Joining



#43: Tubes Joining



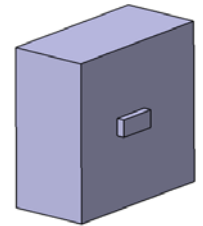
#44; #45: Cylinder and Cube Joining



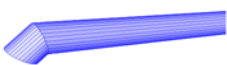
#46: Tubes Joining



#47; #48: Cubes Joining



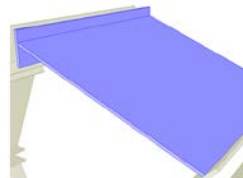
#49: Tubes Joining



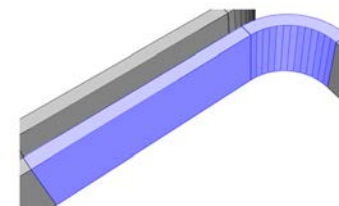
#50: Tubes and Cone Joining



#51: Cubes Joining

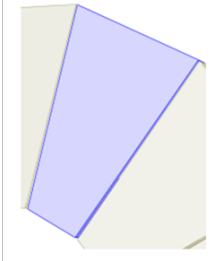


#52 #53: Cube and Tube Joining

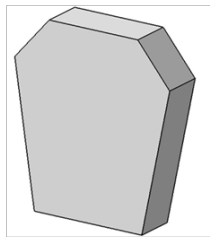


I. Categorization of Geometry

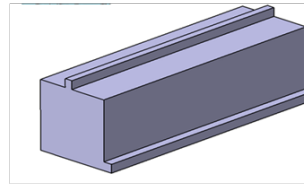
#54: Trapezoid



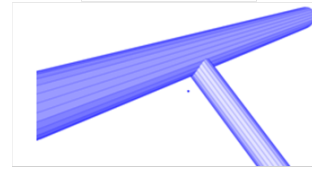
#55: Hexagonal Prism



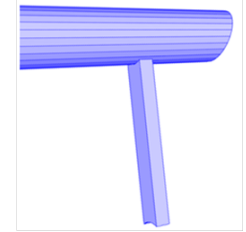
#56: Decagonal Prism



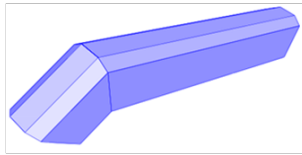
#57: Tubes Joining



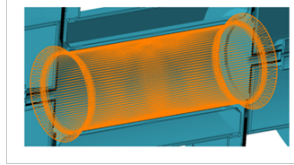
#58 #59: Cube and Tube Joining



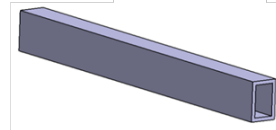
#60 #61: Octagonal Prisms with Cuts Joining



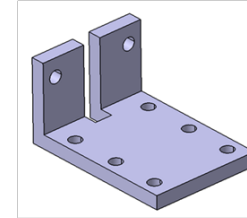
#62: Polycone



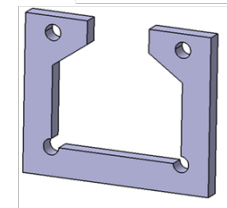
#63: Cube with Cut



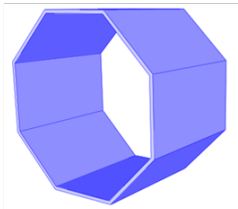
#64: Box with cuts



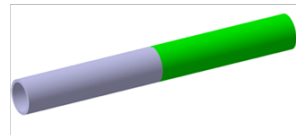
#65: Box with cuts



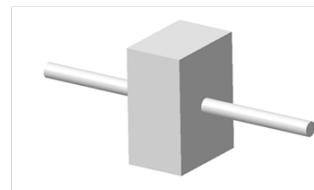
#66: Octagonal prism with cut



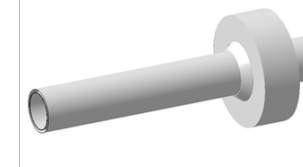
#67: Tubes joining



#68: Tube and Box joining

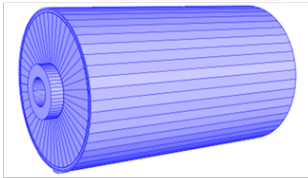


#69: Tubes and Cone Joining

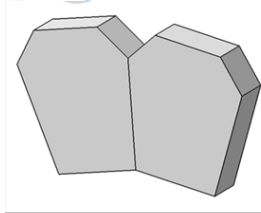


I. Categorization of Geometry

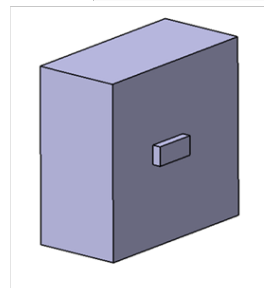
#70: Tubes Joining



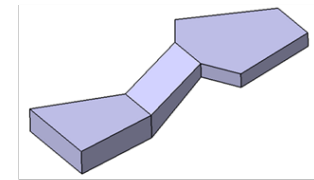
#71: Hexagonal Prism Joining



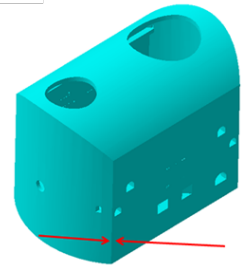
#72: Boxes Joining



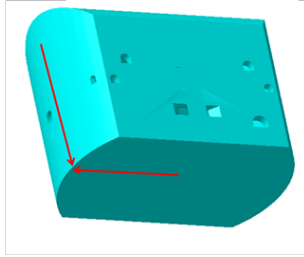
#73: Trapezoid, tetragonal and Hexagonal Prism Joining



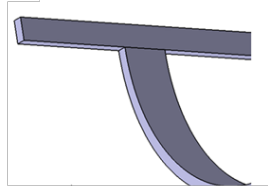
#74: Tubs and Box Joining



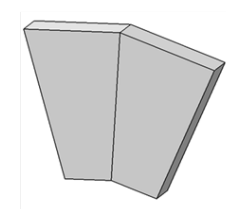
#75: Tubs and Box Joining



#76: Tubs and Box Joining



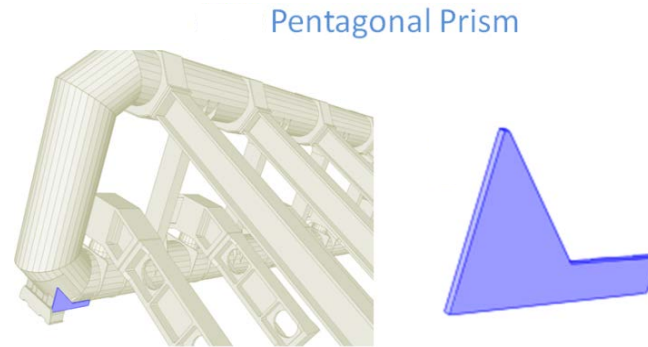
#77: Trapezoids Joining



Part II. Selection of Methods for Description

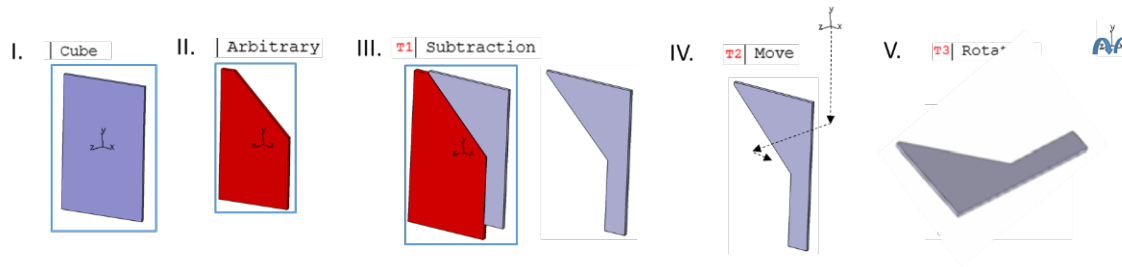
II. Selection of Methods for Description

- Several Methods can be implemented for description of one single object



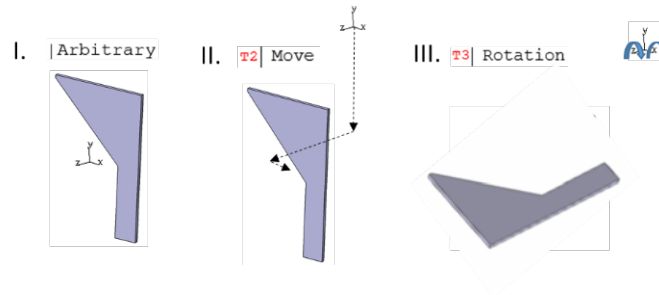
Method 01

- Cube
- Arbitrary
- T1 Subtraction
- T2 Move
- T3 Rotation



Method 02

- Arbitrary
- T1 Move
- T2 Rotation



II. Selection of Methods for Description

Finally, for all above selected typical representatives of object classes of ATLAS detector, full set of possible methods of description were selected:

1st class of 22 objects: 4'460 methods

2nd class of 22 objects: 4'636 methods

3rd class of 33 objects: 6'579 methods

Total: **15'675** methods

II. Selection of Methods for Description

Criteria #01: *Arbitrary_polygon* method should be separated as a standalone method, while

1. Geometry description requires minimal number of Boolean operations and Move/Rotation transactions
2. Geometry can be described directly in position by only Z axis displacement and Z axis rotation.

Example: Descriptions of Octadecagonal Prism



Conclusion: Exclude Methods II and III

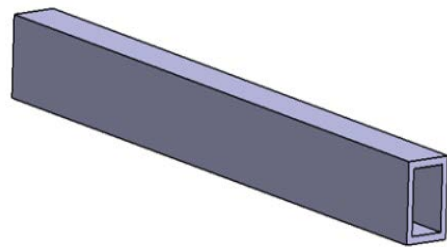
I.	II.	III.
Arbitrary	Cube	Cube
Move (Z)	Arbitrary	Pyramid
Rotation	Subtraction	Move
	Move	Subtraction
	rotation	Cube
		Move
		Subtraction
		Cube
		Move
		Cube
		Move
		Cube
		Move
		Cube
		Pyramid
		Move
		Subtraction
		Union
		Move
		Rotation

II. Selection of Methods for Description

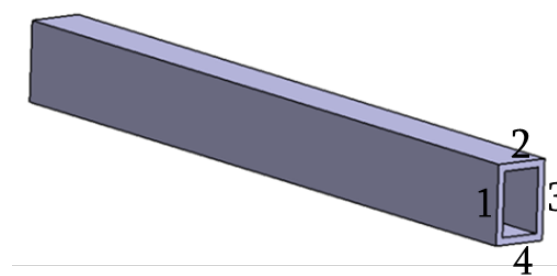
Criteria #02: Minimization of number of used methods in description

1. Ensure compactness of code
2. Reduce number received clashes, contacts and inaccuracies of positioning
3. Ensure better performance by reducing number of regions for consideration during the tracking

Example: Descriptions of Cube with Cut



I.
Cube
Cube
Subtraction
Move
Rotation



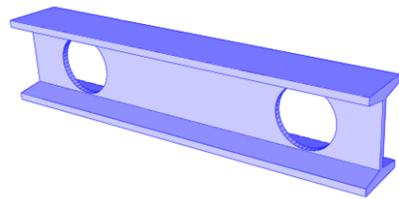
II.
Cube
Move
Cube
Move
Cube
Move
Cube
Move
Union
Move
Rotation

Conclusion: Exclude Method II

II. Selection of Methods for Description

Criteria #03: Exclude descriptions which are using same transactions and methods

Example: Descriptions of Dodecagonal Prism with Cuts



I.

Arbitrary
Tube
Rotation
Move
Subtraction
Rotation
Move
Subtraction
Move (Z)
Rotation

II.

Symmetric
Tube
Rotation
Move
Subtraction
Rotation
Move
Subtraction
Move (Z)
Rotation

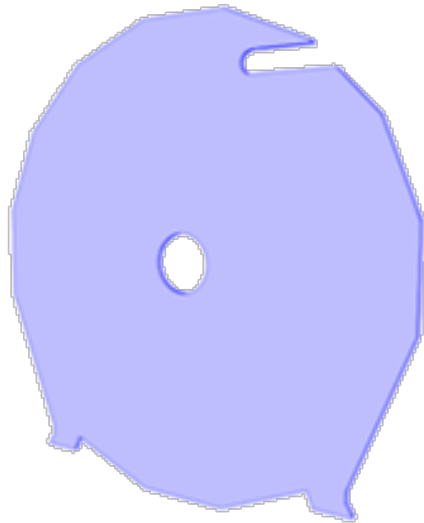
Conclusion: Either I or II should be excluded

II. Selection of Methods for Description

Criteria #04: Exclude descriptions with same consequence of methods

Example: Descriptions of Icositetrahedral prism with cuts

Icositetrahedral Prism with Cuts



I.	II.
Cube	Pyramid
Symmetric	Symmetric
Move	Move
Subtraction	Subtraction
Move	Move
Subtraction	Subtraction
Arbitrary	Arbitrary
Subtraction	Subtraction
Tube	Tube
Move	Move
Subtraction	Subtraction
Cube	Cube
Move	Move
Subtraction	Subtraction
Tube	Tube
Move	Move
Subtraction	Subtraction

Conclusion: Either I or II should be excluded

II. Selection of Methods for Description

- Total number of methods has been analysed and just unique cases of descriptions were selected:

Before Separation

1st class of 22 objects: 4'460 methods

2nd class of 22 objects: 4'636 methods

3rd class of 33 objects: 6'579 methods

Total: **15'675** methods



After Separation

1st class of 22 objects: 11 methods

2nd class of 22 objects: 29 methods

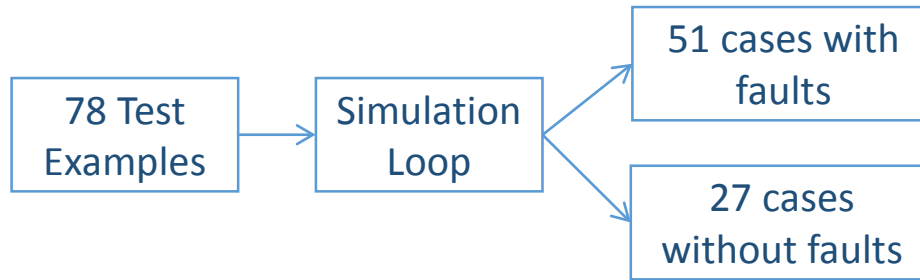
3rd class of 33 objects: 38 methods

Total: **78** methods

Conclusion: 78 unique examples have been formed for the investigation of quality of geometry transformations doing by simulation software.

Part III. Test Runs

III. Test Runs



#	TestExample N	Inaccuracies	Comment
1	1	Yes	Maximal Inaccuracy 0.23 mm
2	2	Yes	Maximal Inaccuracy 0.03 mm
3	3	No	
4	4	Yes	Maximal Inaccuracy 0.51 mm
5	5	No	
6	6	Yes	Maximal Inaccuracy 0.2 mm
7	7		
8	8	Yes	Maximal Inaccuracy 0.01 mm
9	9	Yes	Maximal Inaccuracy 0.01 mm
10	10	Yes	Maximal Inaccuracy 0.03 mm
11	11	Yes	Maximal Inaccuracy 0.09 mm
12	12	Yes	Maximal Inaccuracy 0.09 mm
13	13	Yes	Maximal Inaccuracy 0.04 mm
14	14	Yes	Maximal Inaccuracy 0.05 mm
15	15	Yes	Maximal Inaccuracy 0.01 mm
16	16	Yes	Maximal Inaccuracy 0.03 mm
17	17	Yes	Maximal Inaccuracy 0.04 mm
18	18	Yes	Maximal Inaccuracy 0.19 mm
19	19	Yes	Maximal Inaccuracy 0.06 mm
20	20	Yes	Maximal Inaccuracy 0.15 mm
21	21	No	
22	22	Yes	Maximal Inaccuracy 0.03 mm
23	23	Yes	Maximal Inaccuracy 0.22 mm
24	24	Yes	Inaccuracies on the X and Y Z axes
25	25	Yes	Maximal Inaccuracy 0.18 mm
26	26	Yes	Maximal Inaccuracy 0.19 mm

27	27	Yes	Maximal Inaccuracy 0.12 mm
28	28	Yes	Maximal Inaccuracy 0.12 mm
29	29	Yes	Maximal Inaccuracy 0.05 mm
30	30	Yes	Maximal Inaccuracy 0.03 mm
31	31	Yes	Maximal Inaccuracy 0.03 mm
32	32	Yes	Maximal Inaccuracy 0.06 mm
33	33	Yes	Maximal Inaccuracy 0.06 mm
34	34	Yes	Maximal Inaccuracy 0.01 mm
35	35	Yes	Maximal Inaccuracy 0.01 mm
36	36	Yes	Maximal Inaccuracy 0.01 mm
37	37	Yes	Maximal Inaccuracy 1.52 mm
38	38	Yes	Maximal Inaccuracy 0.03 mm
39	39	Yes	Maximal Inaccuracy 0.04 mm
40	40	Yes	Maximal Inaccuracy 0.14 mm
41	41	Yes	Maximal Inaccuracy 0.14 mm
42	42		
43	43	No	
44	44	Yes	Maximal Inaccuracy 0.01 mm
45	45	Yes	Maximal Inaccuracy 0.01 mm
46	46		
47	47	No	
48	48	No	
49	49		
50	50	No	
51	51	Yes	Maximal Inaccuracy 1.05 mm
52	52	No	

53	53	No	
54			
55	54	No	
56	55	Yes	Maximal Inaccuracy 0.08 mm
57	56	Yes	Maximal Inaccuracy 0.03 mm
58	58	No	
59	59	No	
60	60	No	
61	61	No	
62	62	No	
63	63	Yes	Maximal Inaccuracy 0.12 mm
64	65	No	
65	66	Yes	Maximal Inaccuracy 0.01 mm
66	67	No	
67	68	No	
68	69	No	
69	70	No	
70	71	Yes	Maximal Inaccuracy 0.38 mm
71	72	No	
72	73	No	
73	74	No	
74	75	Yes	Clash 0.89 mm
75	76	Yes	Clash 2.27 mm
76	77	Yes	Clash 0.04 mm
77	78	No	
78	79	No	

T1: XML->GeoMODEL transformation : 43 cases

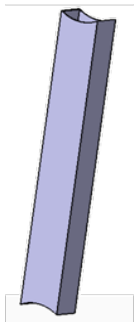
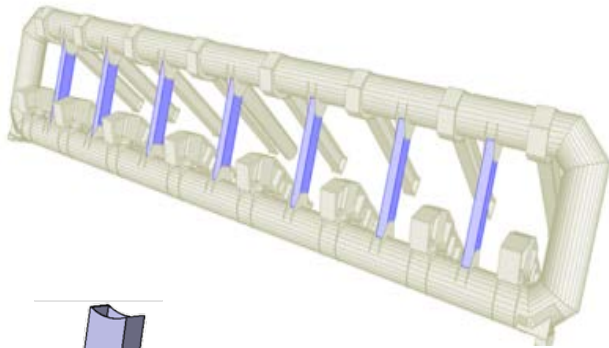
T2: GeoMODEL->GEANT-4 transformation : 8 cases

Part IV. Case Study of Transactions

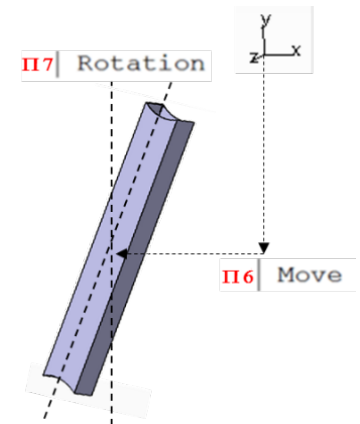
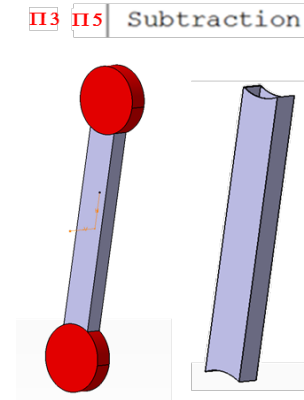
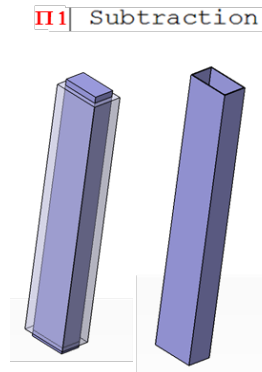
IV. Case Study of Transactions

- Further investigations have done in order to understand reasons which caused inaccurateness
- Geometry transactions *move/rotation* and *Boolean* operations were considered separately and together to discover any kind of correlations between them

Example: Case study of transactions for Tube with cuts

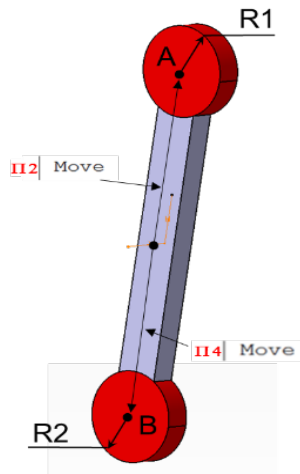


- Cube
- Cube
- III1 Subtraction
- Tube
- II2 Move
- III3 Subtraction
- II4 Move
- III5 Subtraction
- II6 Move
- III7 Rotation



IV. Case Study of Transactions

Sub-Case #01: Π_2/Π_4 movement of A and B center points of auxiliary tubes along Y axis from origin



Results: There are no inaccuracies

	Cube
	Cube
Π_1	Subtraction
	Tube
Π_2	Move
Π_3	Subtraction
Π_4	Move
Π_5	Subtraction
Π_6	Move
Π_7	Rotation

```
<gvsy name="Box1" material="Aluminium" dZ="290.">
  <gvsy_point X_Y="-290.; -8947."/>
  <gvsy_point X_Y="290.; -5187."/>
  <gvsy_point X_Y="250.; -5707."/>
  <gvsy_point X_Y="250.; -8947."/>
</gvsy>

<gvsy name="Box2" material="Aluminium" dZ="270.">
  <gvsy_point X_Y="-240.; -8977."/>
  <gvsy_point X_Y="-240.; -5677."/>
  <gvsy_point X_Y="240.; -5677."/>
  <gvsy_point X_Y="240.; -8977."/>
</gvsy>

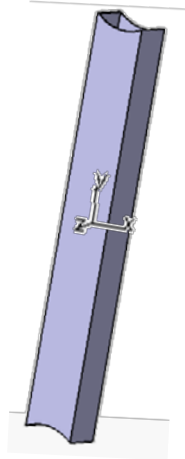
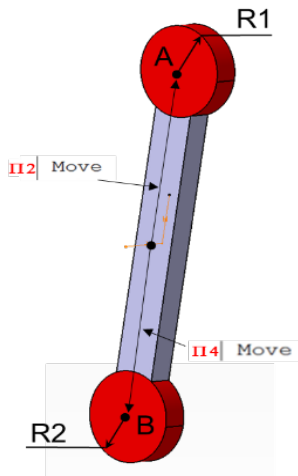
<tube name="Tubel" material="Aluminium" Ric_Z="0.; 544.5; 300." nbPhi="32" />

<composition name="TestExemple02">
  <posXYZ volume="Box1" X_Y_Z="0.; 0.; 0." rot="0.; 0.; 0." />
  <posXYZ volume="Box2" X_Y_Z="0.; 0.; 0." rot="0.; 0.; 0." />
  <posXYZ volume="Tubel" X_Y_Z="0.; -5227.; 0." rot="0.; 0.; 0." />
  <posXYZ volume="Tubel" X_Y_Z="0.; -9427.; 0." rot="0.; 0.; 0." />
</composition>

<composition name="ECT_Toroids">
  <posXYZ volume="TestExemple02" X_Y_Z="0.; 0.; 0." rot="0.; 0.; 0." />
</composition>
```

IV. Case Study of Transactions

Sub-Case #02: Π2/Π4 movement together with Boolean subtractions



- Π1 Cube
- Π2 Cube
- Π3 Subtraction
- Π4 Tube
- Π5 Move
- Π6 Subtraction
- Π7 Move
- Π8 Rotation

```

<gvis name="Box1" material="Aluminium" d2="290.">
  <gvis_point X_Y="-250.; -8947."/ >
  <gvis_point X_Y="-250.; -5707."/ >
  <gvis_point X_Y="250.; -5707."/ >
  <gvis_point X_Y="250.; -8947."/ >
</gvis>

<gvis name="Box2" material="Aluminium" d2="270.">
  <gvis_point X_Y="-240.; -8977."/ >
  <gvis_point X_Y="-240.; -5677."/ >
  <gvis_point X_Y="240.; -5677."/ >
  <gvis_point X_Y="240.; -8977."/ >
</gvis>

<tube name="Tubel" material="Aluminium" Rio_Z="0.; 944.5; 300." nbPhi="32" />

<subtraction name="TestExemple825">
  <posXYZ volume="Box1" X_Y_Z=" 0. ; 0. ; 0. " rot=" 0. ; 0. ; 0. "/>
  <posXYZ volume="Box2" X_Y_Z=" 0. ; 0. ; 0. " rot=" 0. ; 0. ; 0. "/>
  <posXYZ volume="Tubel" X_Y_Z=" 0. ; -5227. ; 0. " rot=" 0. ; 0. ; 0. "/>
  <posXYZ volume="Tubel" X_Y_Z=" 0. ; -9427. ; 0. " rot=" 0. ; 0. ; 0. "/>
</subtraction>

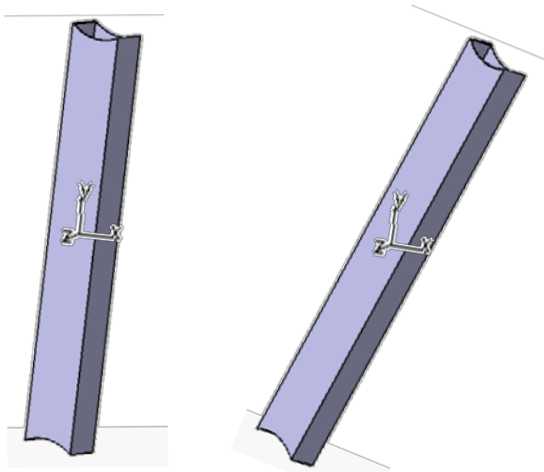
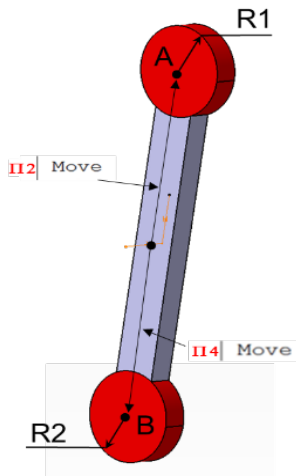
<composition name="ECT_Toroide">
  <posXYZ volume="TestExemple825" X_Y_Z=" 0. ; 0. ; 0. " rot=" 0. ; 0. ; 0. "/>
</composition>
  
```

Results:

		GeoM Δ_1	G-4 Δ_2	Total Δ
A	x	0.03	0	0.03
	y	0.02	0.2	0.22
	z	0	0	0
B	x	0.03	0	0.03
	y	-0.02	0.1	0.08
	z	0	0	0
R1		0	-0.19	-0.19
R2		0	0.1	0.1
<i>Volume</i>		-0.0005	0.0004	-0.0001

IV. Case Study of Transactions

Sub-Case #03: $\Pi 7$ rotation together with $\Pi 2/\Pi 4$ movement and $\Pi 1/\Pi 3$ subtractions



- II1 Cube
- II2 Subtraction
- II3 Tube
- II4 Move
- II5 Subtraction
- II6 Move
- II7 Rotation

```

<gkxy name="Box1" material="Aluminium" d2="290.">
  <qvky_point X_Y="050.; -8947."/>
  <qvky_point X_Y="250.; -8947."/>
  <qvky_point X_Y="250.; -5707."/>
  <qvky_point X_Y="250.; -8947."/>
</gkxy>

<gkxy name="Box2" material="Aluminium" d2="270.">
  <qvky_point X_Y="040.; -8977."/>
  <qvky_point X_Y="240.; -8977."/>
  <qvky_point X_Y="240.; -5677."/>
  <qvky_point X_Y="240.; -8977."/>
</gkxy>

<tube name="Tubel" material="Aluminium" Rio_2="0.; 544.5; 300." nbPhi="32" />

<subtraction name="TestExampleN25">
  <cpaXYZ volume="Box1" X_Y_Z="0; 0.; 0." rot="0.; 0.; 0." />
  <cpaXYZ volume="Box2" X_Y_Z="0; 0.; 0." rot="0.; 0.; 0." />
  <cpaXYZ volume="Tubel" X_Y_Z="0.; -8227.; 0." rot="0.; 0.; 0." />
  <cpaXYZ volume="Tubel" X_Y_Z="0.; -8427.; 0." rot="0.; 0.; 0." />
</subtraction>

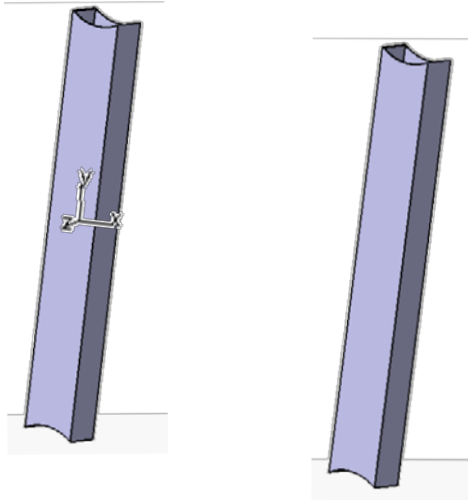
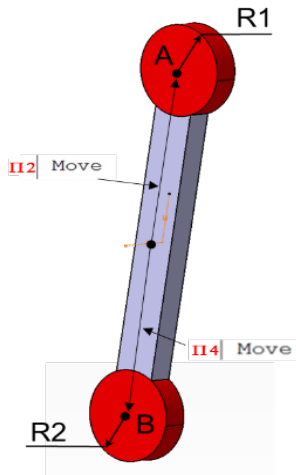
<composition name="ECY_Toroids">
  <cpaXYZ volume="TestExampleN25" X_Y_Z="0.; 0.; 0." rot="0.; 0.; -22.5" />
</composition>
  
```

Results:

		GeoM Δ_1	G-4 Δ_2	Total Δ
A	x	0.05	0.09	0.14
	y	0.01	0.23	0.24
	z	0	0	0
B	x	0.01	0.01	0.02
	y	-0.03	0.02	-0.01
	z	0	0	0
	R1	0	-0.24	-0.24
	R2	0	0.02	0.02
<i>Volume</i>				-0.0001

IV. Case Study of Transactions

Sub-Case #04: Π_6 movement together with Π_2/Π_4 and Π_1/Π_3 subtraction



- Cube
- Cube
- Π_1 Subtraction**
- Π_2 Move**
- Π_3 Subtraction**
- Π_4 Move**
- Π_5 Subtraction**
- Π_6 Move**
- Π_7 Rotation**

```

<gwy name="Box1" material="Aluminium" d2="290.">
  <gwy_point X,Y=":-250.; -8947."/ >
  <gwy_point X,Y=":-250.; -5707."/ >
  <gwy_point X,Y=":250.; -5707."/ >
  <gwy_point X,Y=":250.; -8947."/ >
</gwy>

<gwy name="Box2" material="Aluminium" d2="270.">
  <gwy_point X,Y=":-240.; -8977."/ >
  <gwy_point X,Y=":-240.; -5677."/ >
  <gwy_point X,Y=":240.; -5677."/ >
  <gwy_point X,Y=":240.; -8977."/ >
</gwy>

<tube name="Tubel" material="Aluminium" Ric_2="0.; 544.5; 300." nbPhi="32" />

<subtraction name="TestExampleH25" >
  <posXYZ volume="Box1" X,Y,Z=" 0; 0.; 0. " rot=" 0.; 0.; 0. " />
  <posXYZ volume="Box2" X,Y,Z=" 0; 0.; 0. " rot=" 0.; 0.; 0. " />
  <posXYZ volume="Tubel" X,Y,Z=" 0.; -5227.; 0. " rot=" 0.; 0.; 0. " />
  <posXYZ volume="Tubel" X,Y,Z=" 0.; -9427.; 0. " rot=" 0.; 0.; 0. " />
</subtraction>

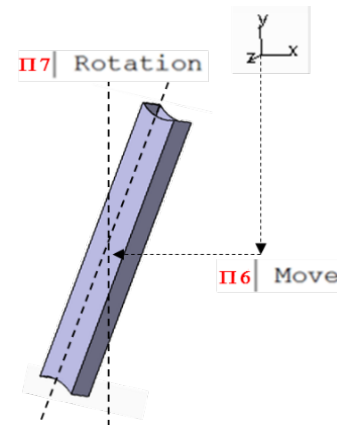
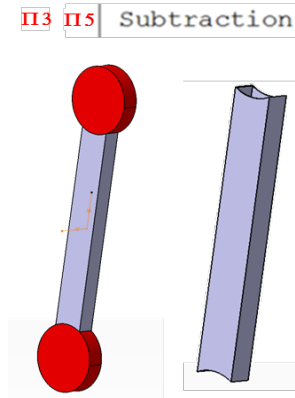
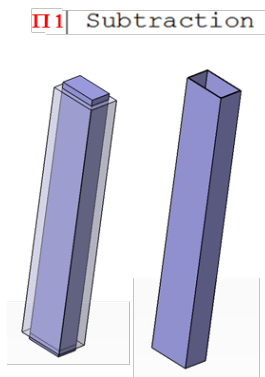
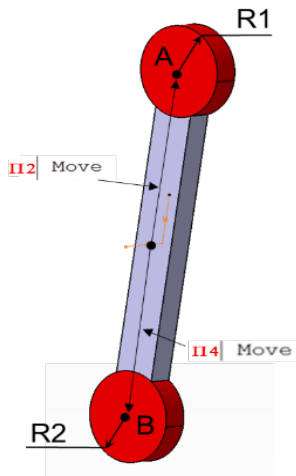
<composition name="ECT_Feroids" >
  <posXYZ volume="TestExampleH25" X,Y,Z=" 0.; 0.; 9540." rot=" 0.; 0.; 0. " />
</composition>
  
```

Results:

		GeoM Δ_1	G-4 Δ_2	Total Δ
A	x	0.03	0.01	0.04
	y	0.02	0.2	0.22
	z	0	0	0
B	x	0.03	0	0.03
	y	-0.03	0.1	0.07
	z	0	0	0
	R1	0.01	-0.2	-0.19
	R2	-0.01	0.1	0.09
Volume				-0.0001

IV. Case Study of Transactions

Sub-Case #05: Π_6 movement together with Π_2/Π_4 ; Π_1/Π_3 subtractions and Π_7 rotation



- Π_1 Subtraction
- Π_2 Move
- Π_3 Subtraction
- Π_4 Move
- Π_5 Subtraction
- Π_6 Move
- Π_7 Rotation

```

<gwy name="Box1" material="Aluminium" d2="290.">
  <gwy_point X_Y="0;0." z="0." rot="0;0;0." />
  <gwy_point X_Y="0;0." z="290." />
  <gwy_point X_Y="290;0." z="0." />
  <gwy_point X_Y="290;0." z="290." />
</gwy>

<gwy name="Box2" material="Aluminium" d2="270.">
  <gwy_point X_Y="0;0." z="0." rot="0;0;0." />
  <gwy_point X_Y="0;0." z="270." />
  <gwy_point X_Y="270;0." z="0." />
  <gwy_point X_Y="270;0." z="270." />
</gwy>

<tube name="Tubel" material="Aluminium" Ric_2="0.; 544.5; 300." nbPhi="32" />

<subtraction name="TestExampleN25" >
  <posXYZ volume="Box1" X_Y_Z="0;0;0." rot="0;0;0." />
  <posXYZ volume="Box2" X_Y_Z="0;0;0." rot="0;0;0." />
  <posXYZ volume="Tubel" X_Y_Z="0;0;0." rot="0;0;0." />
  <posXYZ volume="Tubel" X_Y_Z="0;0;0." rot="0;0;0." />
</subtraction>

<composition name="ECT_Feroids" >
  <posXYZ volume="TestExampleN25" X_Y_Z="0;0;0." rot="0;0;0." />
</composition>
  
```

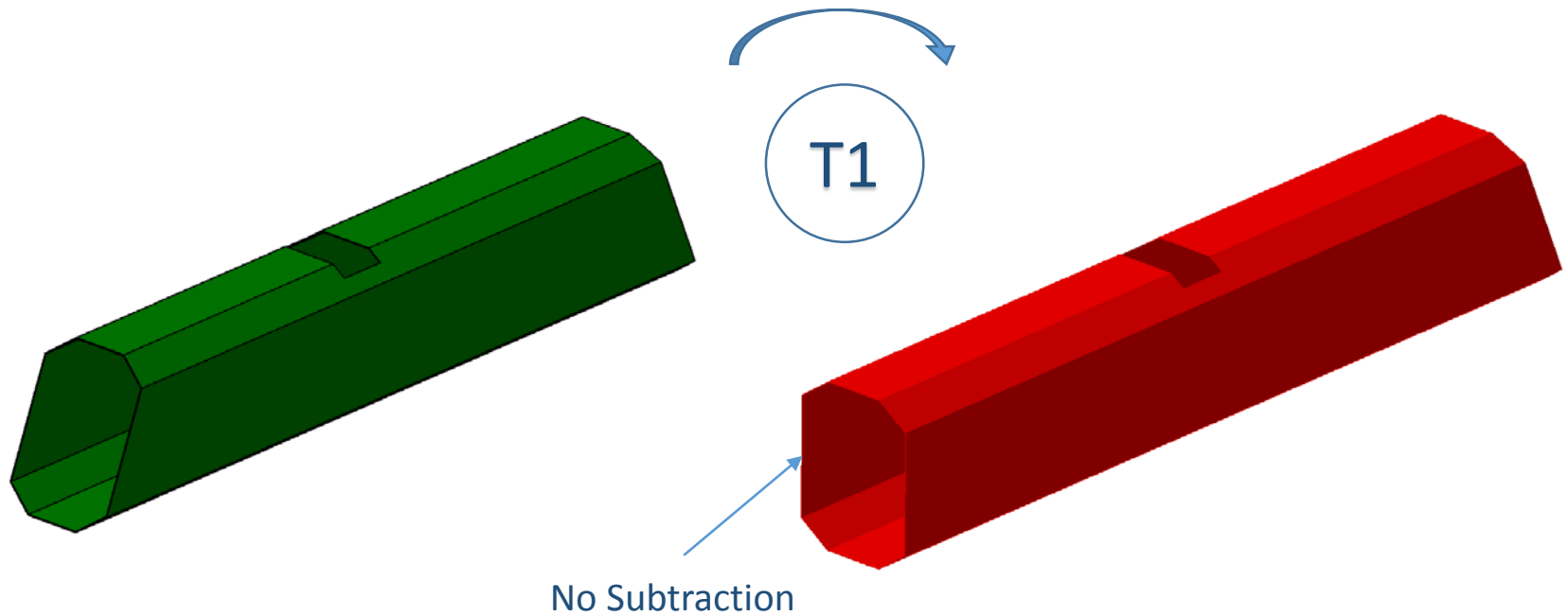
Results:

		GeoM	G-4	Total
		Δ_1	Δ_2	Δ
A	x	0.03	0	0.03
	y	0	-0.02	-0.02
	z	0	0	0
B	x			0.02
	y			0
	z			0
	R1	-0.01	0.18	0.17
	R2			-0.03
Volume		-0.0005	0.0004	-0.0001

IV. Case Study of Transactions

- Direct Faults have been detected

Example: GeoMODEL Boolean Subtraction failure



Part V. Systematization and Learning of Results

V. Systematization and Learning of Results

Ex. №	Geometric Primitives									Transactions					CATIA vs GeoModel (VP1)						CATIA vs Geant4					
	Cube	Tube	Pyr	Trap.	Cone	GeoModel			M	R	Subtr.	M	R	Subtr.	M	R	Conf	M	R	Subtr.	M	R	Conf			
						PolyC.	PolyG.	Arbitr.																Sym.	Dsym	
1	1			3X							5X	4X	5X	X	X	0	0	$\Delta X=0.25$ $\Delta Y=-0.15$ $\Delta V=0.0014$	$\Delta X=-0.02$ $\Delta Y=0.01$	$\Delta X=0.07$ $\Delta Y=-0.18$	0	0	$\Delta X=0.25$ $\Delta Y=-0.15$ $\Delta V=0.0014$	$\Delta X=-0.02$ $\Delta Y=0.01$	$\Delta X=0.06$ $\Delta Y=-0.17$	
2	2	2X									2X	X	2X	X	X	0	0	$\Delta Y=0.01$ $\Delta Z=-0.02$	0	$\Delta X=0.01$	0	0	$\Delta Y=0.01$ $\Delta Z=-0.02$	$\Delta Z=0.03$	$\Delta X=-0.01$ $\Delta Y=-0.02$	
3	4	X												X	X	X			$\Delta X=-0.03$ $\Delta Y=-0.02$	0	$\Delta X=0.02$ $\Delta Y=-0.02$ $\Delta Z=-0.02$			$\Delta X=-0.03$ $\Delta Y=-0.02$	0	$\Delta X=0.02$ $\Delta Y=-0.02$
4	6	2X									X		X	X	X	0		$\Delta X=-0.23$ $\Delta Z=-0.13$ $\Delta V=0.0002$	0	$\Delta X=0.03$ $\Delta Y=0.1$ $\Delta Z=0.01$	0		$\Delta X=-0.23$ $\Delta Z=-0.13$ $\Delta V=0.0002$	$\Delta Z=0.03$	$\Delta X=0.03$ $\Delta Y=0.1$ $\Delta Z=0.01$	
5	7	X											2X	X	X			$\Delta X=-0.07$ $\Delta Y=-0.05$	$\Delta X=0.01$ $\Delta Y=0.05$	$\Delta X=-0.02$ $\Delta Y=0.09$			$\Delta X=-0.07$ $\Delta Y=-0.05$	$\Delta X=0.01$ $\Delta Y=0.05$	$\Delta X=0.04$ $\Delta Y=0.09$	
6	8	2X									X	X	X	X	X	0	0	$\Delta Z=-0.01$	0	0	0	0	$\Delta Z=-0.01$	0	0	
7	9										2X		2X	X	X	0	0		0	$\Delta X=-0.01$			0	0	0	0
8	10	3X									4X		4X	X	X	0		$\Delta X=0.03$ $\Delta Y=0.03$	$\Delta X=0.03$ $\Delta Y=0.03$	$\Delta X=-0.04$ $\Delta Y=-0.02$	0		$\Delta X=0.03$ $\Delta Y=0.03$	$\Delta X=0.03$ $\Delta Y=0.03$	$\Delta X=-0.04$ $\Delta Y=-0.02$	
9	11	2X											X	X	X			$\Delta Y=-0.09$ $\Delta Z=-0.06$	0	$\Delta X=0.03$ $\Delta Y=0.01$			$\Delta Y=-0.09$ $\Delta Z=-0.06$	$\Delta Y=-0.01$ $\Delta Z=0.01$	$\Delta X=0.03$ $\Delta Y=0.02$	
10	12												X	X	X			$\Delta X=-0.09$ $\Delta Y=-0.06$	$\Delta Y=-0.02$	$\Delta X=0.03$ $\Delta Y=0.01$			$\Delta X=-0.09$ $\Delta Y=-0.06$	$\Delta Y=-0.03$	$\Delta X=0.03$ $\Delta Y=0.02$	
11	13	X	X								X		2X	X	X	0		$\Delta X=0.01$ $\Delta V=0.0002$	$\Delta X=-0.03$ $\Delta Y=-0.02$	$\Delta X=-0.01$ $\Delta Y=0.02$			$\Delta X=0.01$ $\Delta V=0.0002$	$\Delta X=0.03$ $\Delta Y=-0.03$	$\Delta X=-0.01$ $\Delta Y=0.03$	
12	14	X	X								2X		2X	X	X	0		$\Delta X=-0.03$ $\Delta Y=-0.02$ $\Delta V=0.0002$	0	$\Delta X=-0.01$ $\Delta Y=0.02$			$\Delta X=-0.03$ $\Delta Y=-0.02$ $\Delta V=0.0002$	0	$\Delta X=-0.01$ $\Delta Y=0.03$	
13	15	X		X							X		X	X	X	0	0		0	$\Delta X=0.01$			0	0	0	$\Delta X=0.01$ $\Delta Y=-0.01$
14	16		X								X		X	X	X	0		$\Delta X=-0.03$ $\Delta Y=-0.02$	0	$\Delta X=-0.01$ $\Delta Y=0.02$			$\Delta X=-0.04$ $\Delta Y=-0.03$	0	$\Delta X=-0.01$ $R=0.01$	
15	17		2X								2X	2X	2X	X	X	0	0	$\Delta X=0.04$ $\Delta Y=0.02$ $\Delta V=0.002$	$\Delta X=0.01$	$\Delta X=0.02$ $\Delta Y=0.03$ $R=0.01$			$\Delta X=0.04$ $R=0.02$ $\Delta V=0.002$	$\Delta X=0.01$ $\Delta Y=0.01$ $\Delta Z=0.01$	$\Delta X=0.02$ $\Delta Y=0.03$ $R=0.05$	
16	18		2X								2X		3X	X		0		$\Delta X=-0.11$ $\Delta Y=0.19$ $\Delta V=0.0003$	0				$\Delta X=-0.11$ $\Delta Y=0.19$ $R=0.01$ $\Delta V=0.0003$	$\Delta X=-0.07$ $\Delta Y=-0.04$ $R=0.08$		

V. Systematization and Learning of Results

Ex. №	Geometric Primitives										Transactions					CATIA vs GeoModel (VP1)						CATIA vs Geant4								
	Cube	Tube	Pyr	Trap.	Cone	GeoModel					M	R	Subt.	M	R	M	R	Subtr.	M	R	Conf	M	R	Subt	M	R	Conf			
						PolyC.	PolyG.	Arbitr.	Sym.	Dsym																				
17	19		2X						X			2X		2X	X	X	0		$\Delta X = -0.06$ $\Delta Y = 0.04$ $R = 0.03$ $\Delta V = -0.0003$	0		$\Delta Y = -0.03$		0		$\Delta X = 0.06$ $\Delta Y = 0.01$ $R = 0.05$ $\Delta V = -0.0003$	$\Delta X = -0.03$ $\Delta Y = -0.04$ $R = 0.05$	$\Delta X = -0.04$ $\Delta Y = 0.06$ $R = 0.09$		
18	20		2X	X						X		3X	X	3X	X	X	0	0	$\Delta X = -0.14$ $\Delta Y = -0.08$ $\Delta V = -0.0003$	$\Delta X = 0.01$ $\Delta Y = 0.01$	$\Delta X = -0.03$ $\Delta Y = 0.06$		0	0	$\Delta X = -0.14$ $\Delta Y = -0.08$ $R = 0.03$ $\Delta V = -0.0003$	$\Delta X = 0.01$ $\Delta Y = -0.04$ $R = 0.03$	$\Delta X = -0.03$ $\Delta Y = 0.06$ $R = 0.01$			
19	22		X						X			X		X	X	X	0		$\Delta X = -0.03$ $\Delta Y = -0.02$ $\Delta V = -0.0001$	0		$\Delta Y = 0.02$		0		$\Delta X = -0.03$ $\Delta Y = -0.02$ $\Delta V = 0.0001$	0		$\Delta Y = 0.02$	
20	23		X	X								X	2X	4X	X	X	0	0	$\Delta X = 0.23$ $\Delta Y = -0.09$ $\Delta V = -0.0001$			$\Delta X = -0.03$ $\Delta Y = -0.09$		0	0	$\Delta X = 0.23$ $\Delta Y = -0.09$ $\Delta V = -0.0001$	0		$\Delta X = -0.03$ $\Delta Y = -0.09$	
21	24	X	X									X		X	X	X	0		$\Delta X = -0.02$ $\Delta Y = 0.01$ $\Delta Z = -0.01$	$\Delta X = -0.01$ $\Delta Y = -0.01$ $\Delta Z = -0.01$	$\Delta X = 0.02$ $\Delta Y = 0.01$		0		$\Delta X = -0.02$ $\Delta Y = 0.01$ $\Delta Z = -0.01$	$\Delta X = -0.02$	$\Delta X = 0.01$ $\Delta Y = 0.02$			
22	25		X									2X		3X	X	X	0		$\Delta X = 0.03$ $\Delta Y = 0.02$ $\Delta V = 0.0005$ $R = 0.01$			$\Delta Y = -0.02$		0		$\Delta X = 0.03$ $\Delta Y = 0.21$ $\Delta V = 0.0001$ $R = 0.17$	0		$\Delta Y = 0.23$ $R = 0.05$	
23	26	2X	X									2X		3X	X	X	0		$\Delta X = 0.03$ $\Delta Y = 0.02$	$\Delta Y = -0.02$ $R = 0.01$	$\Delta X = 0.02$		0		$\Delta X = 0.03$ $\Delta Y = 0.2$ $R = 0.02$	$\Delta Y = -0.01$ $R = 0.02$	$\Delta X = 0.07$ $\Delta Y = -0.03$ $R = 0.05$			
24	27											3X	2X	4X	X	X	0	0	$\Delta X = 0.15$ $\Delta Y = -0.22$ $\Delta Z = -0.06$	$\Delta X = 0.01$ $\Delta Z = -0.02$	$\Delta X = -0.09$ $\Delta Y = 0.07$		0	0	$\Delta X = 0.15$ $\Delta Y = -0.16$ $\Delta Z = 0.08$	$\Delta X = 0.26$ $\Delta Y = 0.03$ $\Delta Z = -0.02$	$\Delta X = -0.07$ $\Delta Y = -0.04$			
25	28	2X										3X	2X	4X	X	X	0	0	$\Delta X = 0.15$ $\Delta Y = -0.22$ $\Delta Z = -0.06$	$\Delta X = 0.01$ $\Delta Z = -0.02$	$\Delta X = -0.09$ $\Delta Y = 0.07$		0	0	$\Delta X = 0.15$ $\Delta Y = -0.16$ $\Delta Z = 0.08$	$\Delta X = 0.26$ $\Delta Y = 0.03$ $\Delta Z = -0.02$	$\Delta X = -0.07$ $\Delta Y = -0.04$			
26	29		X									X	2X	3X	X	X	0	0	$\Delta X = 0.01$ $\Delta Y = -0.03$ $\Delta Z = 0.01$ $\Delta V = 0.0002$	$\Delta Y = -0.01$ $\Delta Z = 0.01$	$\Delta X = -0.01$ $\Delta Y = 0.01$ $\Delta Z = 0.01$		0	0	$\Delta X = 0.01$ $\Delta Y = -0.03$ $\Delta Z = 0.01$ $\Delta V = 0.0002$	$\Delta Y = 0.01$ $\Delta Z = 0.03$	$\Delta X = 0.01$ $\Delta Y = 0.03$ $\Delta Z = -0.01$			
27	30		X									8X	7X	8X	X	X	0	0	$\Delta X = 0.03$ $\Delta Y = -0.03$ $\Delta Z = -0.02$ $\Delta V = 0.0003$	$\Delta Y = -0.03$ $\Delta Z = 0.03$	$\Delta Y = 0.01$ $\Delta Z = 0.04$		0	0	$\Delta X = 0.03$ $\Delta Y = -0.03$ $\Delta Z = 0.03$ $\Delta V = 0.0003$	$\Delta Y = 0.03$ $R = 0.01$	$\Delta X = 0.01$ $\Delta Y = -0.03$ $\Delta Z = 0.02$ $R = 0.01$			

V. Systematization and Learning of of Results

Ex. №	Geometric Primitives										Transactions					CATIA vs GeoModel (VP1)						CATIA vs Geant4						
	Cube	Tube	Pyr	Trap.	Cone	PolyC.	PolyG.	Arbitr.	Sym.	Dsym	M	R	Subt.	M	R	M	R	Subtr.	M	R	Conf	M	R	Subt	M	R	Conf	
28	31	X							X	X	8X	8X	8X	X	X	0	0	$\Delta X=0.03$ $\Delta Y=-0.03$ $\Delta Z=-0.03$ $\Delta_v=0.00031$	$\Delta Y=-0.03$ $\Delta Z=0.03$	$\Delta Y=0.01$ $\Delta Z=0.04$		0	0	$\Delta X=0.03$ $\Delta Y=-0.03$ $\Delta Z=-0.03$ $\Delta_v=0.00031$	$\Delta X=0.02$ $\Delta Y=0.03$ $R=0.01$	$\Delta X=-0.02$ $\Delta Y=-0.03$ $\Delta Z=0.03$ $R=0.01$		
29	32				X						7X	5X	7X	X	X	0	0	$\Delta X=0.03$ $\Delta Y=0.03$ $\Delta Z=0.03$ $\Delta_v=0.0016$	$\Delta X=-0.03$ $\Delta Z=-0.02$ $\Delta_v=0.0033$	$\Delta X=0.01$ $\Delta Z=0.02$		0	0	$\Delta X=-0.05$ $\Delta Y=0.03$ $\Delta Z=-0.03$ $\Delta_v=0.0016$ $R=0.01$	$\Delta X=0.04$ $\Delta Y=0.06$ $\Delta Z=-0.05$ $\Delta_v=0.0033$ $R=0.02$	$\Delta X=-0.05$ $\Delta Y=-0.08$ $\Delta Z=0.02$ $R=0.04$		
30	33				X						7X	5X	7X	X	X	0	0	$\Delta X=0.03$ $\Delta Y=0.03$ $\Delta Z=0.03$ $\Delta_v=0.0016$	$\Delta X=-0.03$ $\Delta Z=-0.02$ $\Delta_v=0.0033$	$\Delta X=0.01$ $\Delta Z=0.02$		0	0	$\Delta X=-0.05$ $\Delta Y=0.03$ $\Delta Z=-0.03$ $\Delta_v=0.0016$ $R=0.01$	$\Delta X=0.04$ $\Delta Y=0.06$ $\Delta Z=-0.05$ $\Delta_v=0.0033$ $R=0.02$	$\Delta X=-0.05$ $\Delta Y=-0.08$ $\Delta Z=0.02$ $R=0.04$		
31	34		X								2X	2X	2X	X	X	0	0	$\Delta_v=0.0001$	0	0		0	0	$\Delta Y=0.01$ $\Delta_v=0.0001$	0	0		
32	35		X						X		2X	2X	2X	X	X	0	0	$\Delta_v=0.0001$	0	0		0	0	$\Delta Y=0.01$ $\Delta_v=0.0001$	0	0		
33	36		X								2X		2X	X	X	0		$\Delta X=0.02$ $\Delta_v=0.00001$	0	$\Delta X=-0.01$ $\Delta Z=-0.01$		0		$\Delta X=0.02$ $\Delta Z=0.01$ $\Delta_v=0.00007$	$\Delta X=0.02$ $\Delta Z=-0.02$ $R=0.03$	$\Delta X=-0.17$ $\Delta Z=0.17$ $R=0.25$		
34	37	2X	2X								3X		3X	X	X	0		$\Delta X=0.01$ $\Delta Z=0.01$ $\Delta_v=0.00007$	0	$\Delta Z=0.02$		0		$\Delta X=0.02$ $\Delta Z=0.01$	$\Delta X=-0.03$ $\Delta Z=0.05$ $R=0.05$	$\Delta X=-0.16$ $\Delta Z=-0.21$ $R=0.19$		
35	38		2X							X		2X	X			0		$\Delta X=-0.03$ $\Delta Y=-0.03$ $\Delta V=0.0009$	0			0		$\Delta X=-0.03$ $\Delta Y=-0.03$ $\Delta V=0.0009$	0			
36	39	X	2X								2X		4X	X		0		$\Delta X=-0.24$ $\Delta Y=-0.18$ $\Delta V=0.0009$	0			0		$\Delta X=-0.24$ $\Delta Y=-0.18$ $\Delta V=0.0009$	0			
37	40											2X	4X	X	X	0		$\Delta X=0.11$ $\Delta Y=0.09$ $\Delta Z=-0.12$ $\Delta_v=0.0004$	$\Delta X=0.01$ $\Delta Y=-0.01$ $\Delta Z=0.01$	$\Delta X=0.09$ $\Delta Y=0.1$		0		$\Delta X=0.11$ $\Delta Y=0.09$ $\Delta Z=-0.12$ $\Delta_v=0.0004$	$\Delta X=0.01$ $\Delta Y=0.01$ $\Delta Z=0.01$	$\Delta X=0.09$ $\Delta Y=0.1$		
38	41	X										3X	4X	X	X	0		$\Delta X=0.11$ $\Delta Y=0.09$ $\Delta Z=-0.12$ $\Delta_v=0.0004$	$\Delta Y=0.01$	$\Delta X=0.09$ $\Delta Y=0.1$		0		$\Delta X=0.11$ $\Delta Y=0.09$ $\Delta Z=-0.12$ $\Delta_v=0.0004$	$\Delta Y=0.01$	$\Delta X=0.09$ $\Delta Y=0.1$		

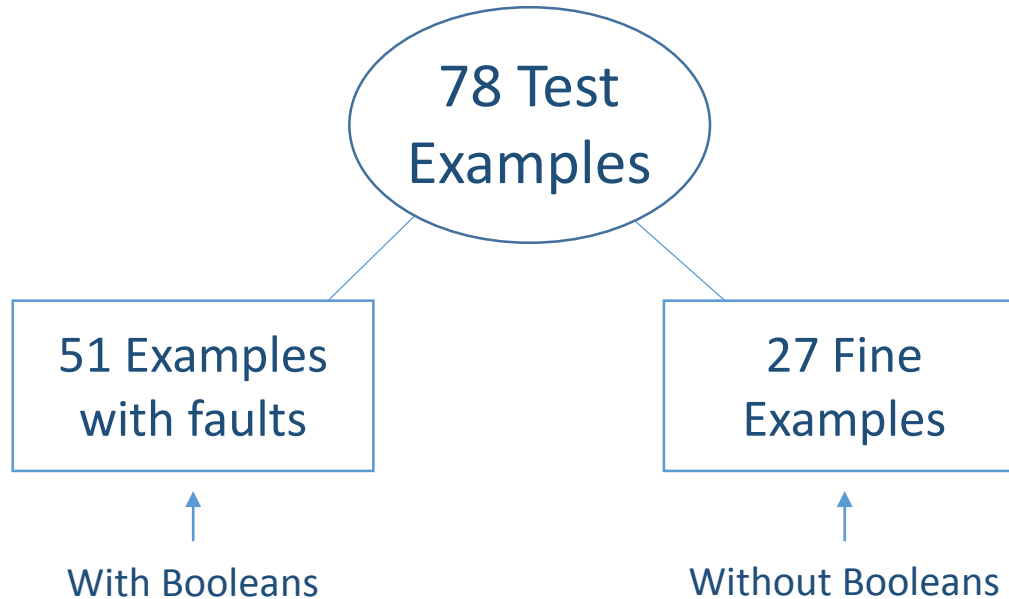
V. Systematization and Learning of Results

Ex. №	Geometric Primitives										Transactions					CATIA vs GeoModel (VP1)					CATIA vs Geant4							
	Cube	Tube	Pyr	Trap.	Cone	GeoModel					M	R	Subt.	M	R	M	R	Subtr.	M	R	Conf	M	R	Subt	M	R	Conf	
						PolyC.	PolyG.	Arbitr.	Sym.	Dsym																		
39	55	X			X							2X	2X	2X	X	X	0	0	$\Delta X=0.08$ $\Delta Y=0.01$	$\Delta Y=0.02$	$\Delta X=-0.01$ $\Delta Y=0.02$	-	0	0	$\Delta X=0.08$ $\Delta Y=0.01$	$\Delta Y=0.02$	$\Delta X=-0.01$ $\Delta Y=0.01$	-
40	56	2X										3X		3X	X	X	0		$\Delta X=0.03$ $\Delta Y=0.02$	0	$\Delta X=0.01$	-	0		$\Delta X=0.03$ $\Delta Y=0.02$	0	0	-
41	57		2X									2X	2X	X	X	X	0	0	$\Delta X=0.04$ $\Delta Y=0.02$ $\Delta V=0.002$	$\Delta X=0.01$	$\Delta X=0.02$ $\Delta Y=0.03$ $R=0.01$		0	0	$\Delta X=0.04$ $R=0.02$ $\Delta V=0.002$	$\Delta X=0.01$ $\Delta Y=0.01$ $\Delta Z=0.01$	$\Delta X=0.02$ $\Delta Y=0.03$ $\Delta Z=0.05$	-
42	58	2X	X									X		2X	2X	X	0		$\Delta X=0.03$ $\Delta Y=0.02$	$\Delta Y=-0.02$ $R=0.01$	$\Delta X=0.02$		0		$\Delta X=0.03$ $\Delta Y=0.2$ $R=0.02$	$\Delta Y=-0.01$ $R=0.02$	$\Delta X=0.07$ $\Delta Y=-0.03$ $R=0.05$	-
43	59	2X	X									X		2X	2X	X	0		$\Delta X=0.03$ $\Delta Y=0.02$ $\Delta_v=0.0005$ $R=0.01$	0	$\Delta Y=-0.02$		0		$\Delta X=0.03$ $\Delta Y=0.21$ $\Delta_v=0.0001$ $R=0.17$	0	$\Delta Y=0.23$ $R=0.05$	-
44	60	X								2X		X	X	2X	2X	2X	0	0	$\Delta X=0.15$ $\Delta Y=-0.22$ $\Delta Z=-0.06$	$\Delta X=0.01$ $\Delta Z=-0.02$	$\Delta X=-0.09$ $\Delta Y=0.07$		0	0	$\Delta X=0.15$ $\Delta Y=-0.16$ $\Delta Z=0.08$	$\Delta X=0.26$ $\Delta Y=0.03$ $\Delta Z=-0.02$	$\Delta X=-0.07$ $\Delta Y=-0.04$	-
45	61											X	X	2X	2X	2X	0	0	$\Delta X=0.15$ $\Delta Y=-0.22$ $\Delta Z=-0.06$	$\Delta X=0.01$ $\Delta Z=-0.02$	$\Delta X=-0.09$ $\Delta Y=0.07$		0	0	$\Delta X=0.15$ $\Delta Y=-0.16$ $\Delta Z=0.08$	$\Delta X=0.26$ $\Delta Y=0.03$ $\Delta Z=-0.02$	$\Delta X=-0.07$ $\Delta Y=-0.04$	-
46	63	2X												X	X	X	0		$\Delta Y=-0.09$ $\Delta Z=0.06$	$\Delta Z=0.01$	$\Delta X=0.03$ $\Delta Y=0.01$	-	0		$\Delta X=0.09$ $\Delta Z=0.06$	$\Delta Y=-0.01$ $\Delta Z=0.01$	$\Delta X=0.03$ $\Delta Y=0.02$	-
47	69	X	X									X		X	X		0		$\Delta X=-0.06$ $\Delta Y=-0.05$	0		-	0		$\Delta X=-0.06$ $\Delta Y=-0.05$	0		-
48	72	X			X							3X	3X	2X	X	X	0	0	$\Delta X=0.08$ $\Delta Y=0.01$	$\Delta Y=0.02$	$\Delta X=-0.01$ $\Delta Y=0.02$	0	0	0	$\Delta X=0.08$ $\Delta Y=0.01$	$\Delta Y=0.02$	$\Delta X=-0.01$ $\Delta Y=0.01$	0
49	74	4X			2X							6X	6X	5X	2X	2X	0	0	$\Delta X=0.08$ $\Delta Y=0.01$	$\Delta Y=0.02$	$\Delta X=-0.01$ $\Delta Y=0.02$	-	0	0	$\Delta X=0.08$ $\Delta Y=0.01$	$\Delta Y=0.02$	$\Delta X=-0.01$ $\Delta Y=0.01$	-
50	75	2X	X									2X		X		X	0		$\Delta X=-1.34$ $\Delta Z=0.94$ $\Delta_v=0.175$		$\Delta X=-0.47$ $\Delta Z=0.33$	Clash= 1.28	0		$\Delta X=-1.44$ $\Delta Z=-0.9$ $\Delta_v=0.044$		$\Delta Z=-0.09$	Clash= 0.91
51	77	X	2X									X	X	X	X	X	0		$\Delta X=-1.71$ $\Delta Z=-1.25$ $\Delta_v=34.45$	0	0	-	0	0	$\Delta X=-1.75$ $\Delta Z=-1.25$ $R=0.05$ $\Delta V=34.45$	0		-

V. Systematization and Learning of Results

Postulate #01

- For all type of detector geometries dimensional, form and positioning faults are caused by *Boolean* operations

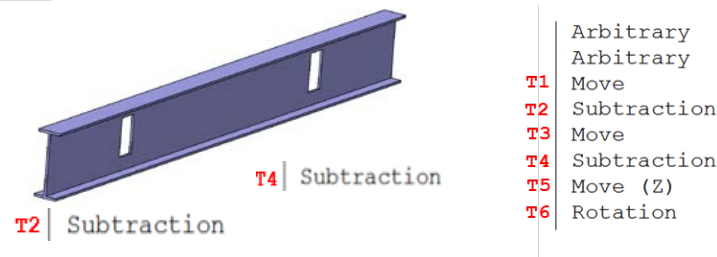


V. Systematization and Learning of Results

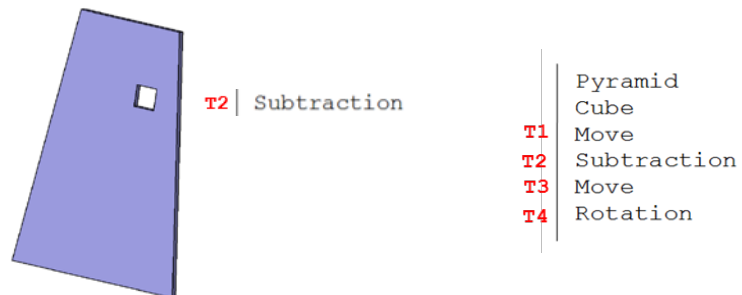
Postulate #02

- All internal surfaces received by *Boolean* subtraction of parametrical primitives from Box brings 0 faults

- Test Example #09



- Test Example #15



V. Systematization and Learning of Results

Postulate #03

- Boolean operations are correlate with *Move* and *Rotate* transactions executing after the *Boolean*. All *Move/Rotate* transactions before *Boolean* are fine

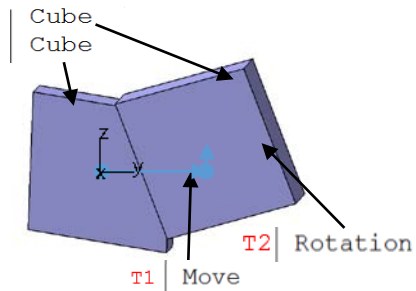
Ex. No	Geometric Primitives										Transactions					CATIA vs GeoModel (VP1)						CATIA vs Geant4					
	Cube	Tube	Pyr	Trap.	Cone	PolyC.	PolyG.	Arbitr.	Sym.	Dsym	M	R	Subtr.	M	R	Subtr.	M	R	Conf	M	R	Subt	M	R	Conf		
1	1			3X							5X	4X	5X	X	X	0	0	$\Delta X=0.25$ $\Delta Y=-0.15$ $\Delta V=0.0014$	$\Delta X=-0.02$ $\Delta Y=0.01$	$\Delta X=0.07$ $\Delta Y=-0.18$	0	0	$\Delta X=0.25$ $\Delta Y=-0.15$ $\Delta V=0.0014$	$\Delta X=-0.02$ $\Delta Y=0.01$	$\Delta X=0.06$ $\Delta Y=-0.17$	0	0
2	2	2X								2X	X	2X	X	X	0	0	$\Delta Y=0.01$ $\Delta Z=-0.02$	0	$\Delta X=0.01$	0	0	$\Delta Y=0.01$ $\Delta Z=-0.02$	$\Delta Z=0.03$	$\Delta X=-0.01$ $\Delta Y=-0.02$	0	0	
3	4	X						X				X	X	X	0	0	$\Delta X=-0.03$ $\Delta Y=-0.02$	0	$\Delta X=0.02$ $\Delta Y=-0.02$ $\Delta Z=-0.02$	0	0	$\Delta X=-0.03$ $\Delta Y=-0.02$	0	$\Delta X=0.02$ $\Delta Y=-0.02$	0	0	
4	6	2X								X		X	X	X	0	0	$\Delta X=-0.23$ $\Delta Z=-0.13$ $\Delta V=0.0002$	0	$\Delta X=0.03$ $\Delta Y=0.1$ $\Delta Z=0.01$	0	0	$\Delta X=-0.23$ $\Delta Z=-0.13$ $\Delta V=0.0002$	$\Delta Z=0.03$	$\Delta X=0.03$ $\Delta Y=0.1$ $\Delta Z=0.01$	0	0	
5	7	X						X				2X	X	X	0	0	$\Delta X=-0.07$ $\Delta Y=-0.05$	$\Delta X=0.01$ $\Delta Y=0.05$	$\Delta X=-0.02$ $\Delta Y=0.09$	0	0	$\Delta X=-0.07$ $\Delta Y=-0.05$	$\Delta X=0.01$ $\Delta Y=0.05$	$\Delta X=0.04$ $\Delta Y=0.09$	0	0	
6	8	2X								X	X	X	X	X	0	0	$\Delta Z=-0.01$	0	0	0	0	$\Delta Z=-0.01$	0	0	0	0	
7	9							2X		2X		2X	X	X	0	0	0	0	$\Delta X=-0.01$	0	0	0	0	0	0	0	
8	10	3X								4X		4X	X	X	0	0	$\Delta X=0.03$ $\Delta Y=0.03$	$\Delta X=0.03$ $\Delta Y=0.03$	$\Delta X=-0.04$ $\Delta Y=-0.02$	0	0	$\Delta X=0.03$ $\Delta Y=0.03$	$\Delta X=0.03$ $\Delta Y=0.03$	$\Delta X=-0.04$ $\Delta Y=-0.02$	0	0	
9	11	2X										X	X	X	0	0	$\Delta Y=-0.09$ $\Delta Z=-0.06$	0	$\Delta X=0.03$ $\Delta Z=0.01$	0	0	$\Delta Y=-0.09$ $\Delta Z=-0.06$	$\Delta Y=-0.01$ $\Delta Z=0.01$	$\Delta X=0.03$ $\Delta Y=0.02$	0	0	
10	12							2X				X	X	X	0	0	$\Delta X=-0.09$ $\Delta Y=-0.06$	$\Delta Y=-0.02$	$\Delta X=0.03$ $\Delta Y=0.01$	0	0	$\Delta X=-0.09$ $\Delta Y=-0.06$	$\Delta Y=-0.03$	$\Delta X=0.03$ $\Delta Y=0.02$	0	0	
11	13	X	X						X	X		2X	X	X	0	0	$\Delta X=0.01$ $\Delta V=0.0002$	$\Delta X=-0.03$ $\Delta Y=-0.02$	$\Delta X=-0.01$ $\Delta Y=0.02$	0	0	$\Delta X=0.01$ $\Delta V=0.0002$	$\Delta X=0.03$ $\Delta Y=-0.03$	$\Delta X=-0.01$ $\Delta Y=0.03$	0	0	
12	14	X	X					X		2X		2X	X	X	0	0	$\Delta X=-0.03$ $\Delta Y=-0.02$ $\Delta V=0.0002$	0	$\Delta X=-0.01$ $\Delta Y=0.02$	0	0	$\Delta X=-0.03$ $\Delta Y=-0.02$ $\Delta V=0.0002$	0	$\Delta X=-0.01$ $\Delta Y=0.03$	0	0	

V. Systematization and Learning of Results

Postulate #04

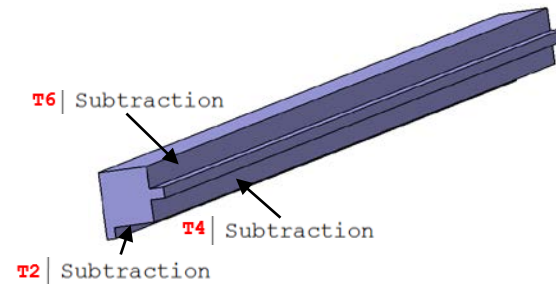
- For all external surfaces created by subtraction of parametrical primitives from Box, *Boolean* operation don't correlated with *Move/Rotation* transactions

Test Example #08



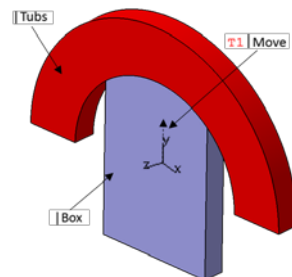
Cube
Cube
T1 Move
T2 Rotation
T3 Subtraction
T4 Move
T5 Rotation

Test Example #56



Box
Box
T1 Move
T2 Subtraction
T3 Move
T4 Subtraction
T5 Move
T6 Subtraction
T7 Move
T8 Rotation

Test Example #77



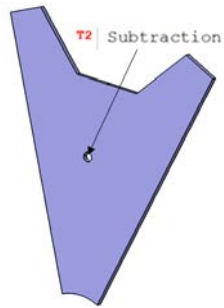
Box
Tubs
T1 Move
T2 Subtraction
T3 Move
T4 Rotation
Tubs
T5 Rotation

V. Systematization and Learning of Results

Postulate #05

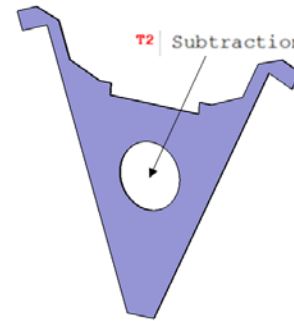
- For some internal surfaces created by subtraction of parametrical primitives from Polygon methods, *Boolean* operation don't correlated with *Move* transactions

Test Example #19, #20



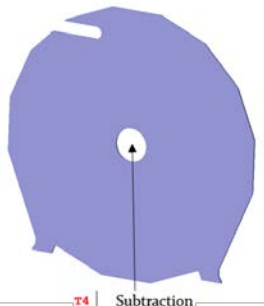
	Arbitrary
	Tube
T1	Move
T2	Subtraction
	Tube
T3	Move
T4	Subtraction
T5	Rotation
T6	Move

Test Example #22



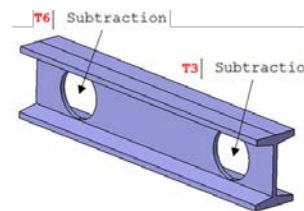
	Arbitrary
	Tube
T1	Move
T2	Subtraction
T3	Move (Z)
T4	Rotation

Test Example #38, #39



	Symmetric
	Arbitrary
T1	Subtraction
	Cube
T2	Move
T3	Subtraction
	Tube
T4	Subtraction
	Tube
T5	Move
T6	Subtraction
T7	Move

Test Example #34, #35



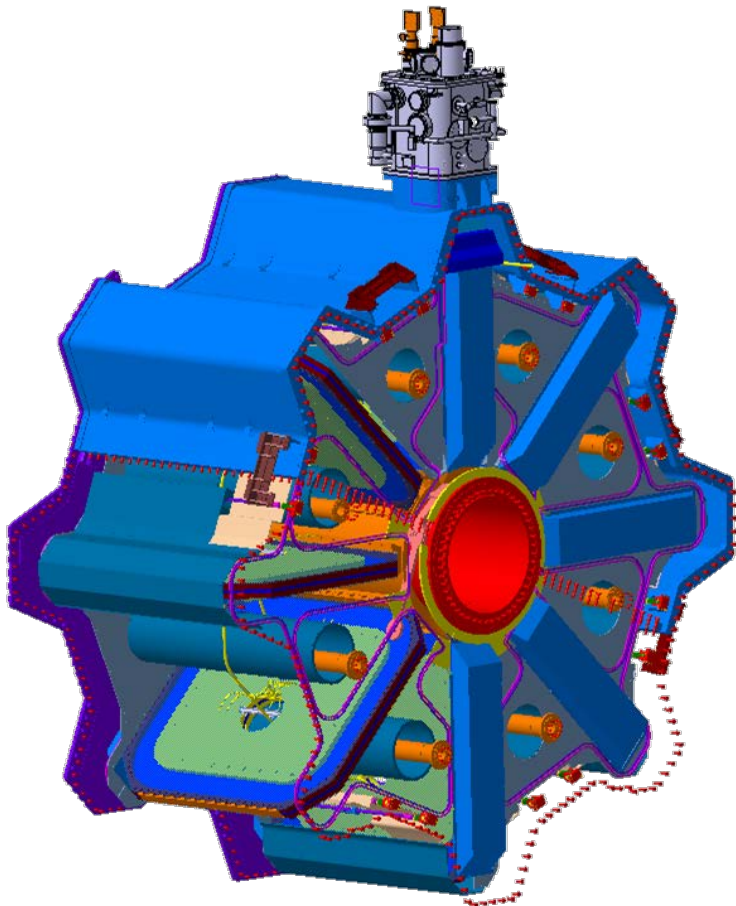
	Arbitrary
	Tube
T1	Rotation
T2	Move
T3	Subtraction
T4	Rotation
T5	Move
T6	Subtraction
T7	Move (Z)
T8	Rotation

Checking Hypothesis 02:

Investigation of as-built
geometry descriptions with
geometry descriptions of
simulation

ATLAS End-CAP Toroid Study

- ATLAS End-CAP toroid Magnet Assembly is the heaviest component of Detector. Weight is 280t

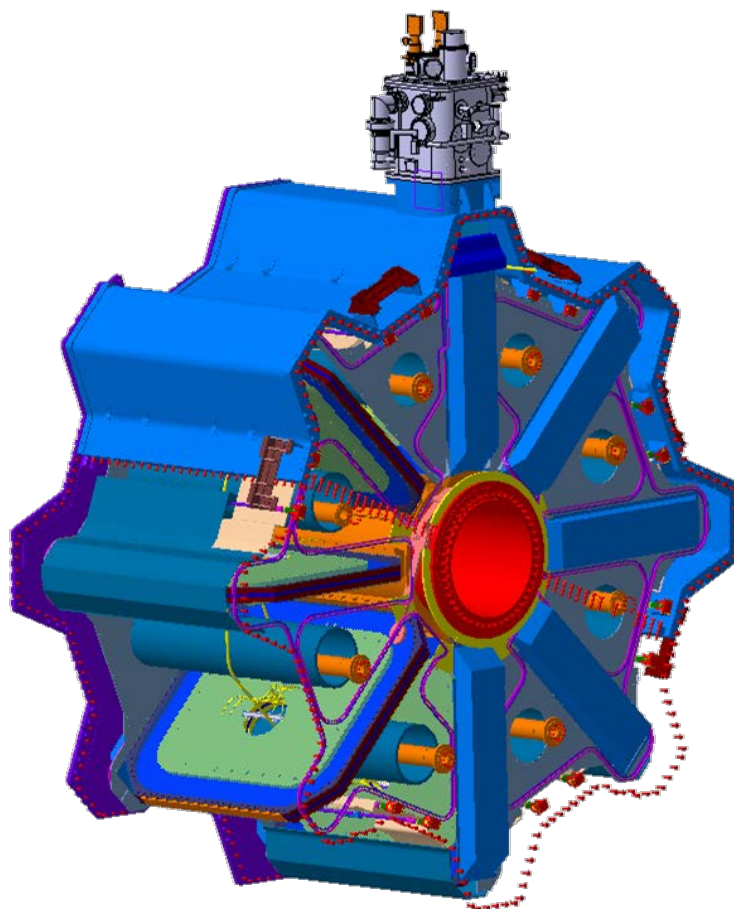


ATLAS End-CAP Toroid Study

Source geometry has been taken from SmarTeam Engineering Database:

Path : ATLAS CURRENT/Detector System/Magnets ATLAS/Toroid Magnets ATLAS/Barrel Toroid Magnet ATLAS/End-cap Toroid Magnet
Model: ST0268528 ECT assembly side C (id: CAD000628534)

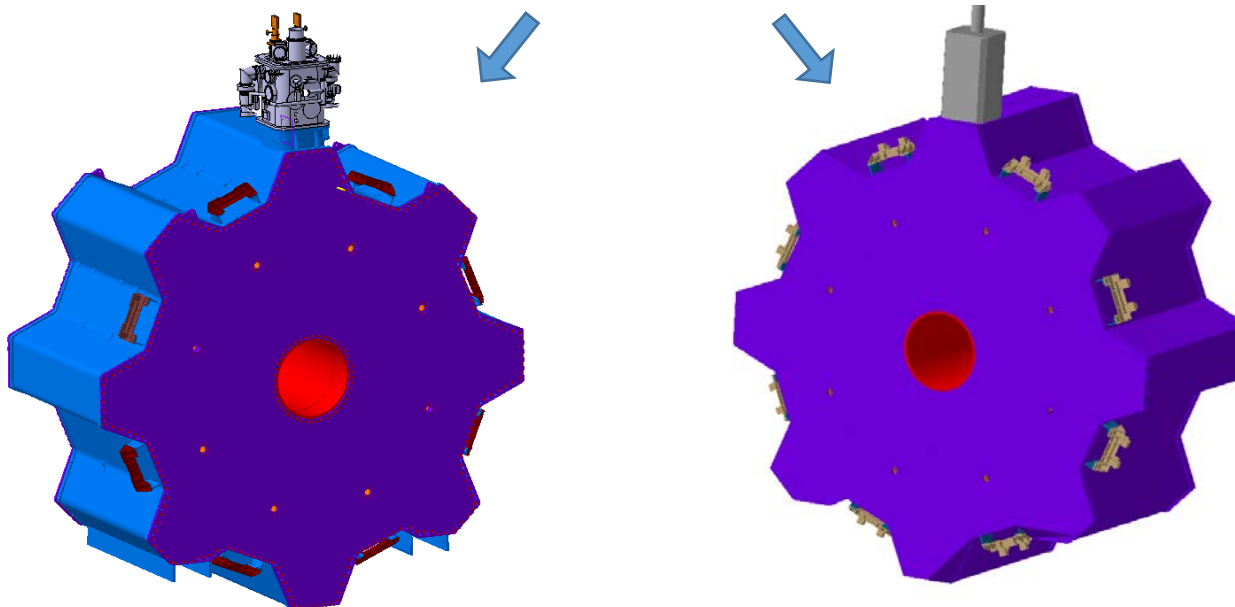
Missing parts have been created from CDD Drawings (902 drawings):



		<i>Drawings Added</i>
Vacuum vessel	1 Cover	90
	2 Shield	219
	3 Tie Rods	64
	4 Bore Tube	4
	5 Turret	268
Cold Mass	6 Coil	4
	7 Keystone box	27
	8 Services	135
	9 Supports	13
	10 Joke	12
	11 Tower	30

ATLAS End-CAP Toroid Study

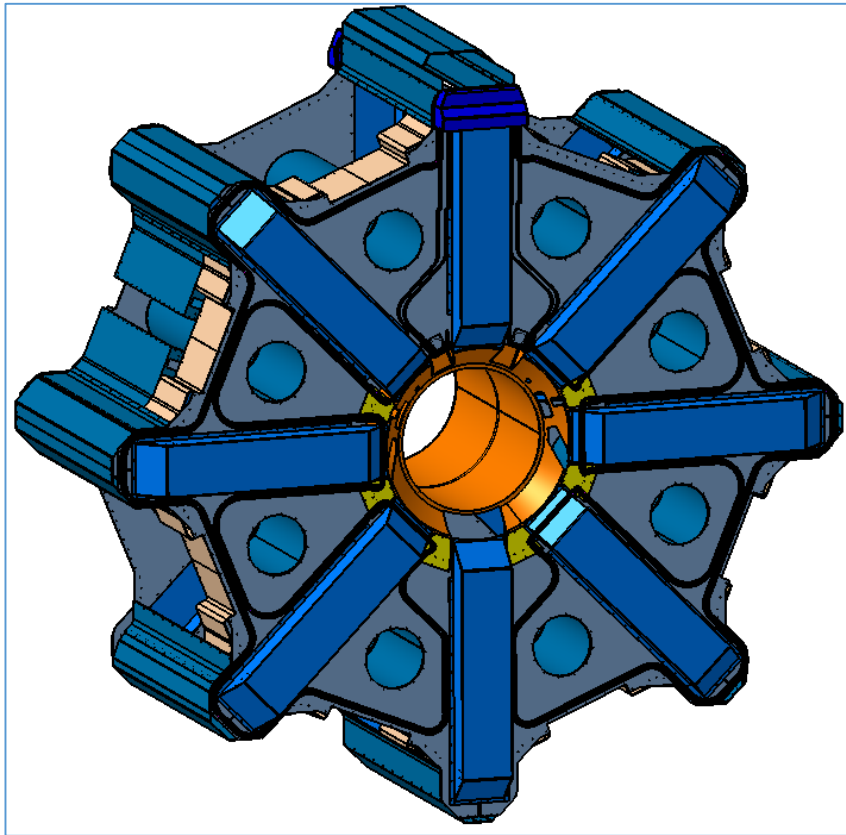
	CATIA	XML	Difference	%
1 Cold Mass	116740 kgs	123012 kgs	+6'272 kgs	5.4 %
2 Thermal Shielding	15988 kgs	15957 kgs	-31 kgs	0.2 %
3 Cover	57966 kgs	57185 kgs	-781 kgs	1.3 %
4 Bore Tube	13433 kgs	10208 kgs	-3'225 kgs	24.0 %
5 Yoke	1820 kgs	1338 kgs	-483 kgs	26.5 %
6 Stay Tube	2028 kgs	2214 kgs	+186 kgs	9.2 %
7 JTV Shielding	4161 kgs	4510 kgs	+349 kgs	8.4 %
8 Turret	2476 kgs	1512 kgs	-964 kgs	38.9 %
9 Tie Rod	3077 kgs	1268 kgs	-1'809 kgs	58.8 %
10 Bolts/	2965 kgs		-2'965 kgs	100.0 %
11 Services	869 kgs		-869 kgs	100.0 %



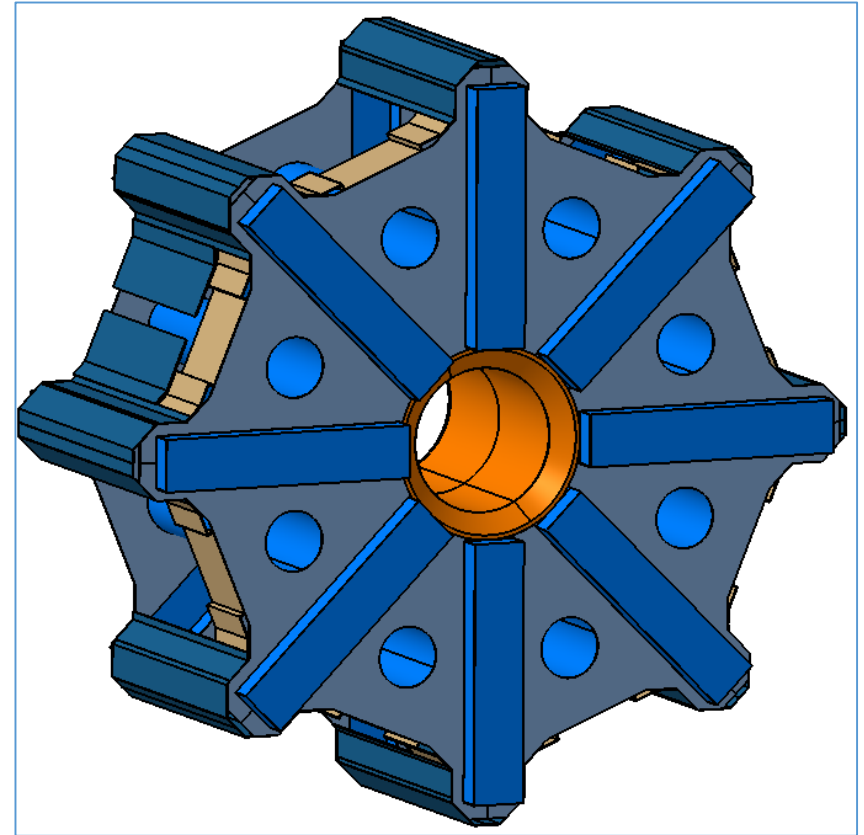
Simplification/Thermal Shielding Assembly

	Detailed	Simplified		Detailed	Simplified		Material	
	Volume/ m ³	Volume/ m ³	Difference/ m ³	Mass/ kgs	Mass/ kgs	Difference/ kgs		Density
Thermal Silding	6,057	6,056	0,001	16`353,9	16`351,2	2,7	Aluminum	2700

Detailed model



Simplifield model



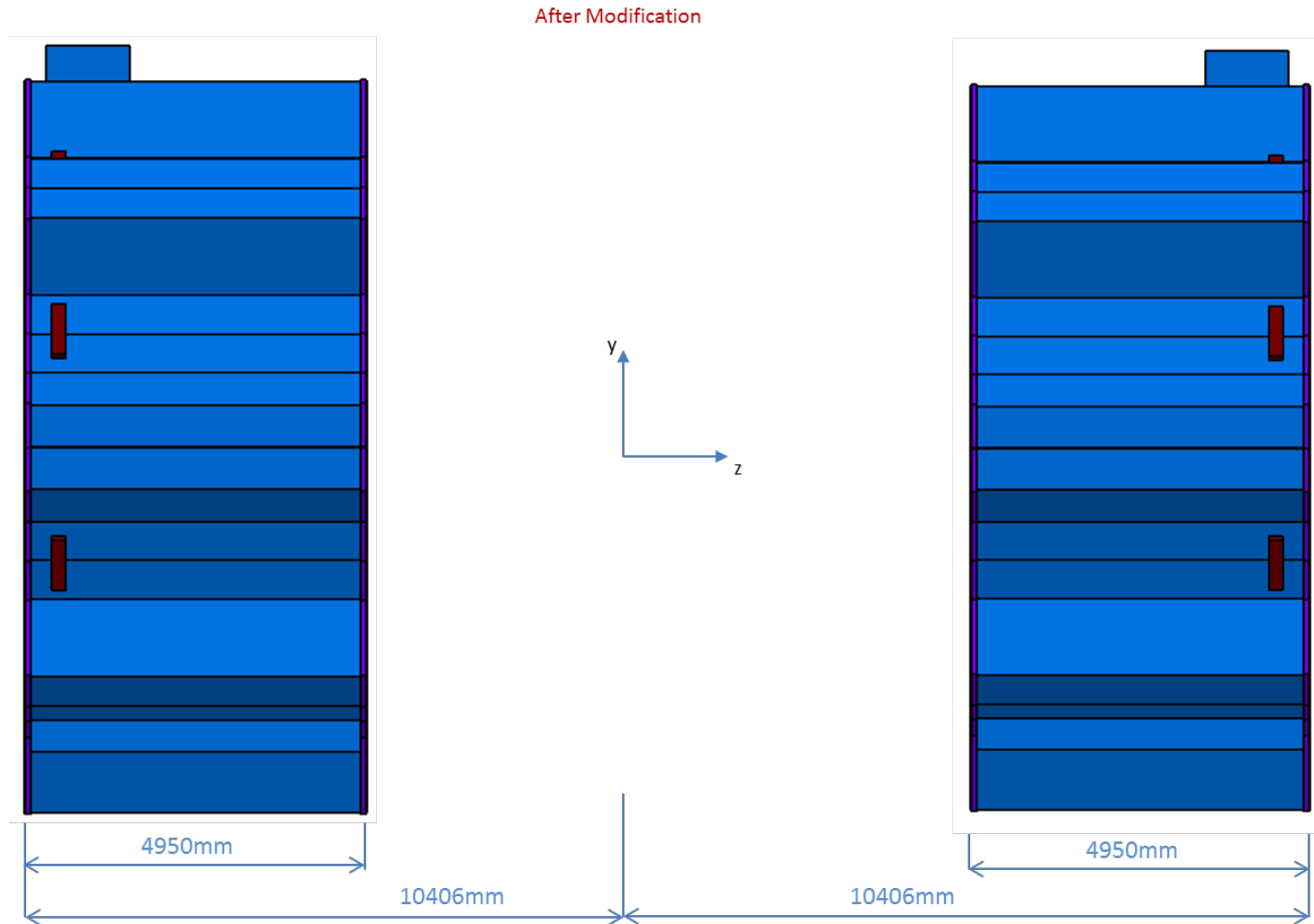
ATLAS End-CAP Toroid Study / Simplification

- Results of Simplification of End-CAT Toroid Assemblies

	Detailed	Simplified		Detailed	Simplified		Material	
	Volume/ m ³	Volume/ m ³	Difference/ m ³	Mass/ kgs	Mass/ kgs	Difference/ kgs		Density
Cold Mass	43,24	43,23	0,01	116`748	116`721	27	Aluminum	2700
Thermal Silding	6,057	6,056	0,001	16`353	16`351	2	Aluminum	2700
Cover	20,8	20,804	-0,004	56`160	56`170,8	-10,8	Aluminum	2700
Brackets	0,22	0,2201	-0,0001	1760	1760,8	-0,8	Steel	8000
BoreTube	1,679	1,678	0,001	13`432	13`424	8	Steel	8000
Yoke	0,231	0,231	0	1848	1848	0	Steel	8000
Stay Tube	0,751	0,751	0	2027,7	2027,7	0	Aluminum	2700
JTV Shilding	1,65	1,649	0,001	4158	4155,48	2,52	Polyboron	2520
Tie Rod	0,393	0,393	0	3144	3144	0	Steel	8000
Bolts/	0,371	0,371	0	2968	2968	0	Steel	8000
Services	0,06	0,06	0	480	480	0	Steel	8000

ATLAS End-CAP Toroid Study / Conflicts Checking

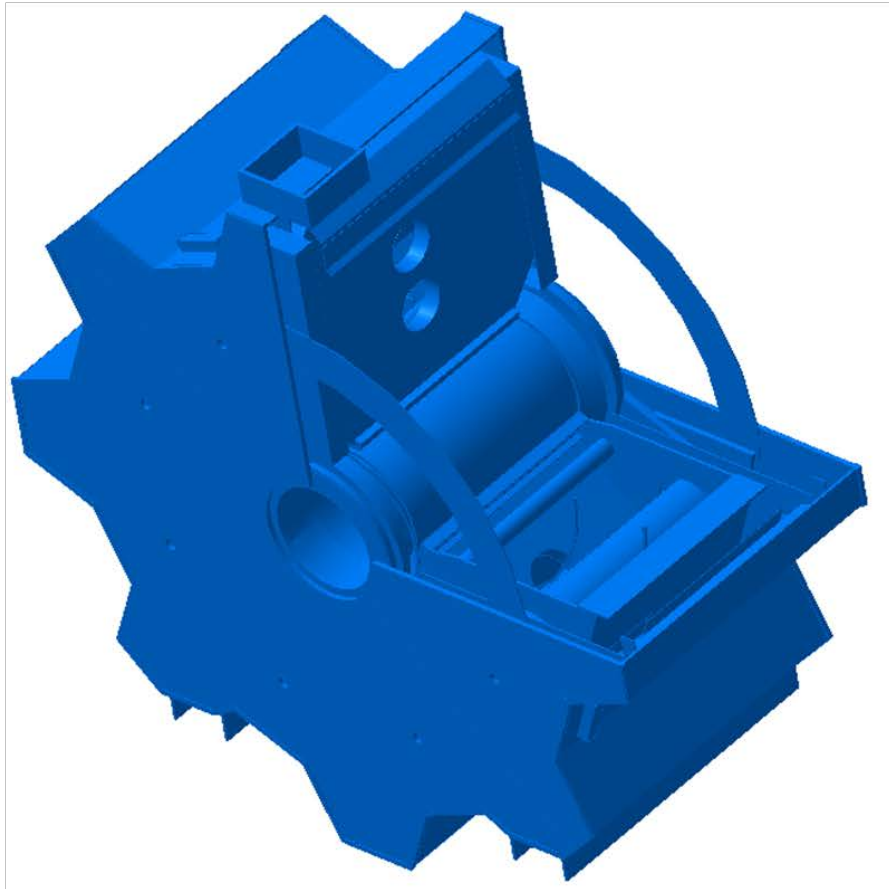
- ECT Cover *as-built* model



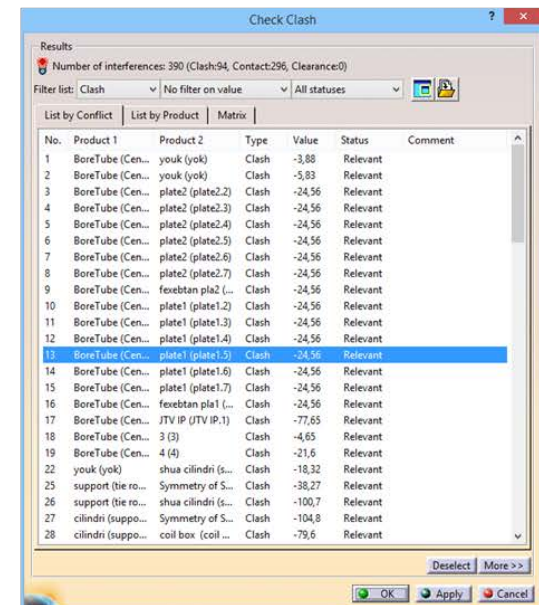
ATLAS End-CAP Toroid Study / Conflicts Checking

Internal Conflicts of ECT

ECT After Modification



There Was Internal Conflicts



Check Clash

Results
Number of interferences: 390 (Clash:94, Contact:296, Clearance:0)

Filter list: Clash No filter on value All statuses

List by Conflict | List by Product | Matrix

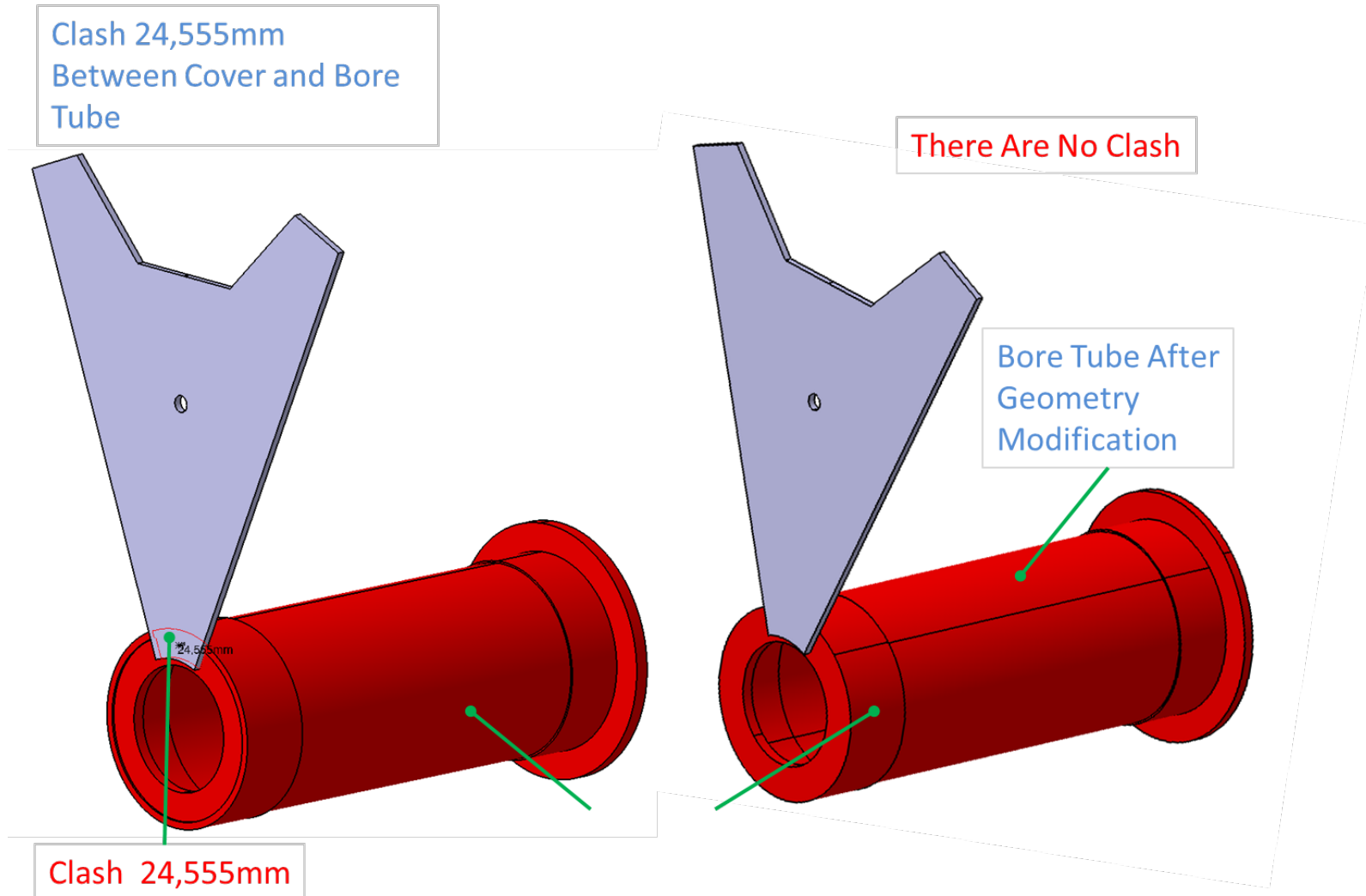
No.	Product 1	Product 2	Type	Value	Status	Comment
1	BoreTube (Cen...	youk (yok)	Clash	-3,88	Relevant	
2	BoreTube (Cen...	youk (yok)	Clash	-5,83	Relevant	
3	BoreTube (Cen...	plate2 (plate2.2)	Clash	-24,56	Relevant	
4	BoreTube (Cen...	plate2 (plate2.3)	Clash	-24,56	Relevant	
5	BoreTube (Cen...	plate2 (plate2.4)	Clash	-24,56	Relevant	
6	BoreTube (Cen...	plate2 (plate2.5)	Clash	-24,56	Relevant	
7	BoreTube (Cen...	plate2 (plate2.6)	Clash	-24,56	Relevant	
8	BoreTube (Cen...	plate2 (plate2.7)	Clash	-24,56	Relevant	
9	BoreTube (Cen...	fexebtan pla2 (...)	Clash	-24,56	Relevant	
10	BoreTube (Cen...	plate1 (plate1.2)	Clash	-24,56	Relevant	
11	BoreTube (Cen...	plate1 (plate1.3)	Clash	-24,56	Relevant	
12	BoreTube (Cen...	plate1 (plate1.4)	Clash	-24,56	Relevant	
13	BoreTube (Cen...	plate1 (plate1.5)	Clash	-24,56	Relevant	
14	BoreTube (Cen...	plate1 (plate1.6)	Clash	-24,56	Relevant	
15	BoreTube (Cen...	plate1 (plate1.7)	Clash	-24,56	Relevant	
16	BoreTube (Cen...	fexebtan pla1 (...)	Clash	-24,56	Relevant	
17	BoreTube (Cen...	JTV IP (JTV IP.1)	Clash	-77,65	Relevant	
18	BoreTube (Cen...	3 (3)	Clash	-4,65	Relevant	
19	BoreTube (Cen...	4 (4)	Clash	-21,6	Relevant	
22	youk (yok)	shua cilindri (s...	Clash	-18,32	Relevant	
25	support (tie ro...	Symmetry of S...	Clash	-38,27	Relevant	
26	support (tie ro...	shua cilindri (s...	Clash	-100,7	Relevant	
27	cilindri (suppo...	Symmetry of S...	Clash	-104,8	Relevant	
28	cilindri (suppo...	coil box (coil ...)	Clash	-79,6	Relevant	

Deselect More >>

OK Apply Cancel

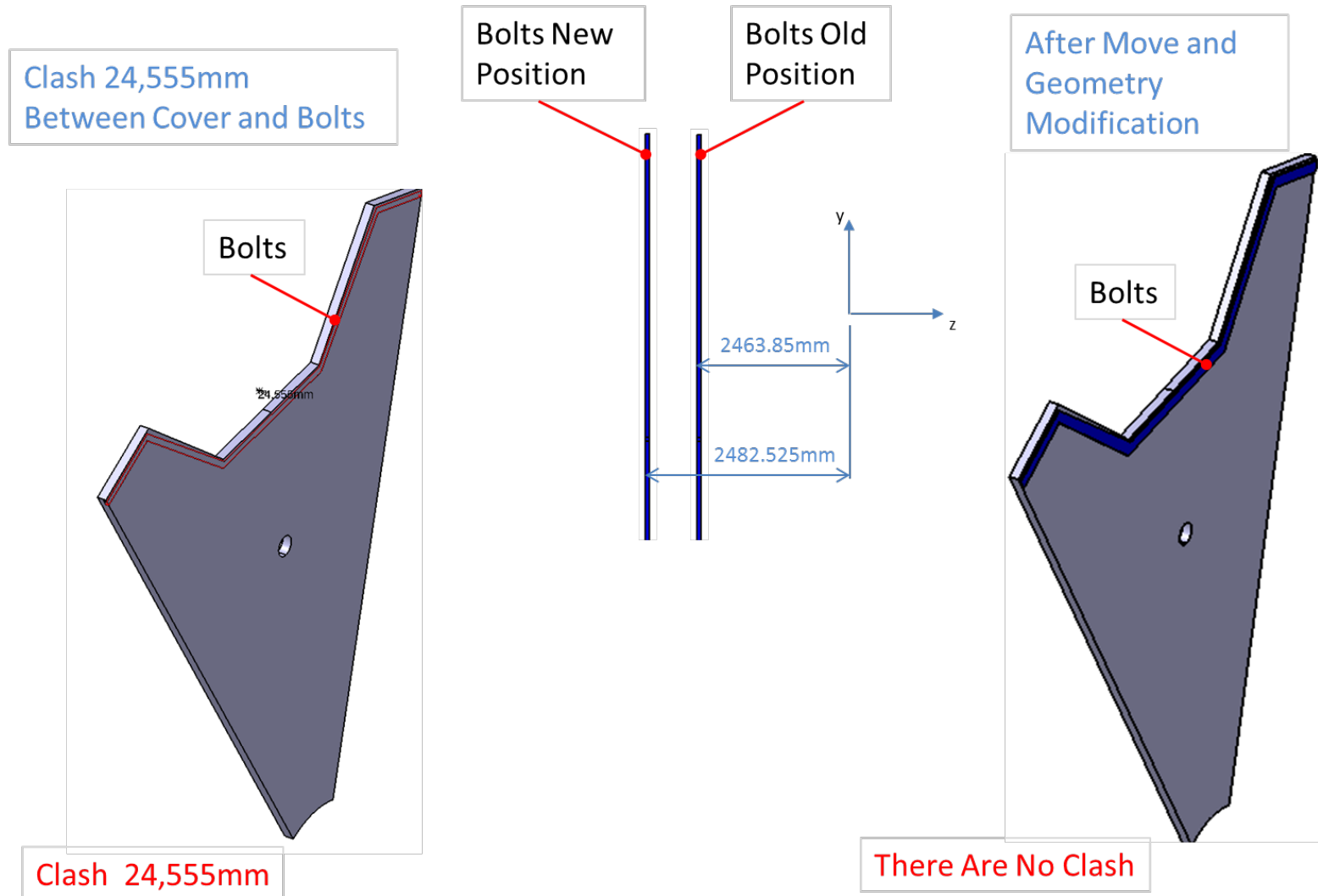
ATLAS End-CAP Toroid Study / Conflicts Checking

Internal Conflicts of ECT



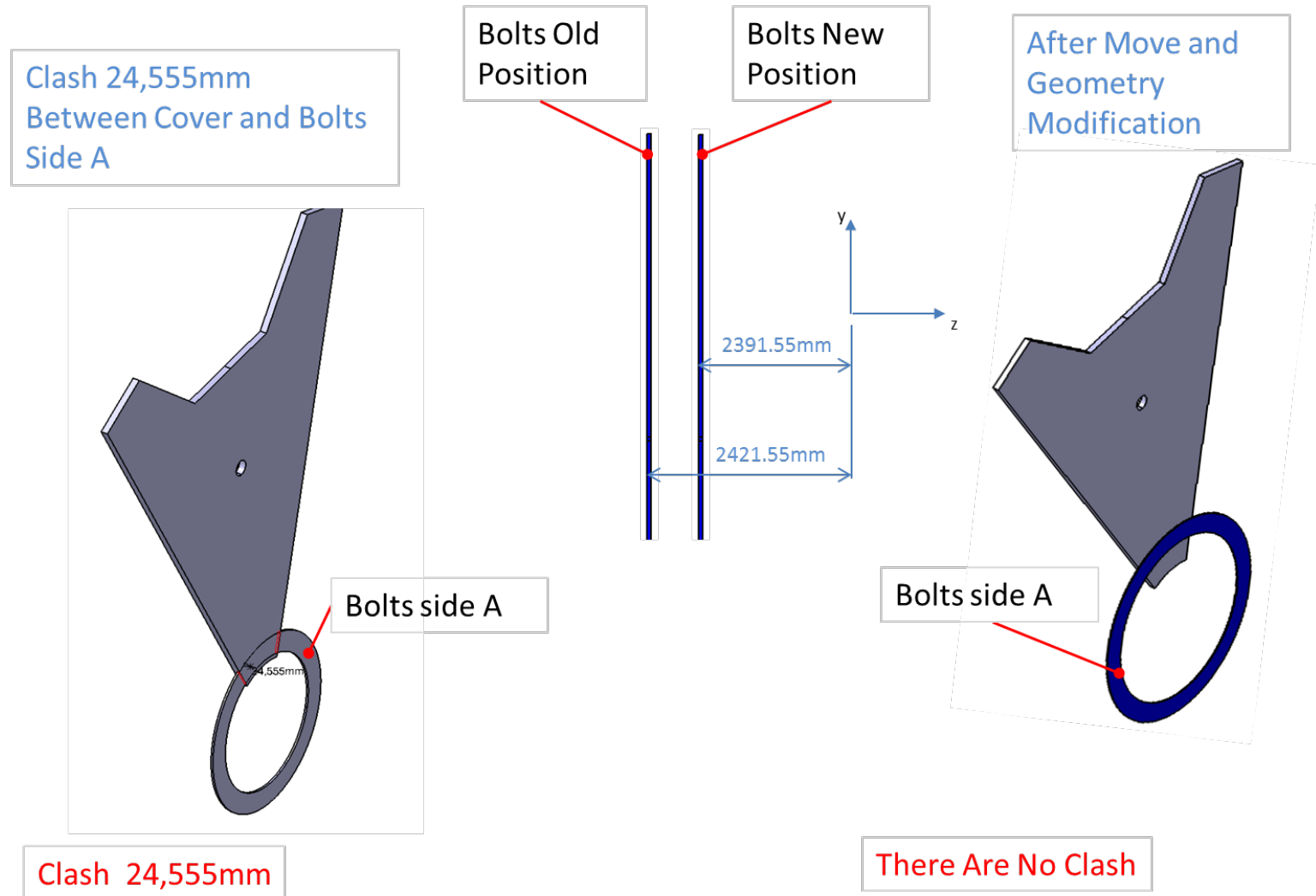
ATLAS End-CAP Toroid Study / Conflicts Checking

Internal Conflicts of ECT



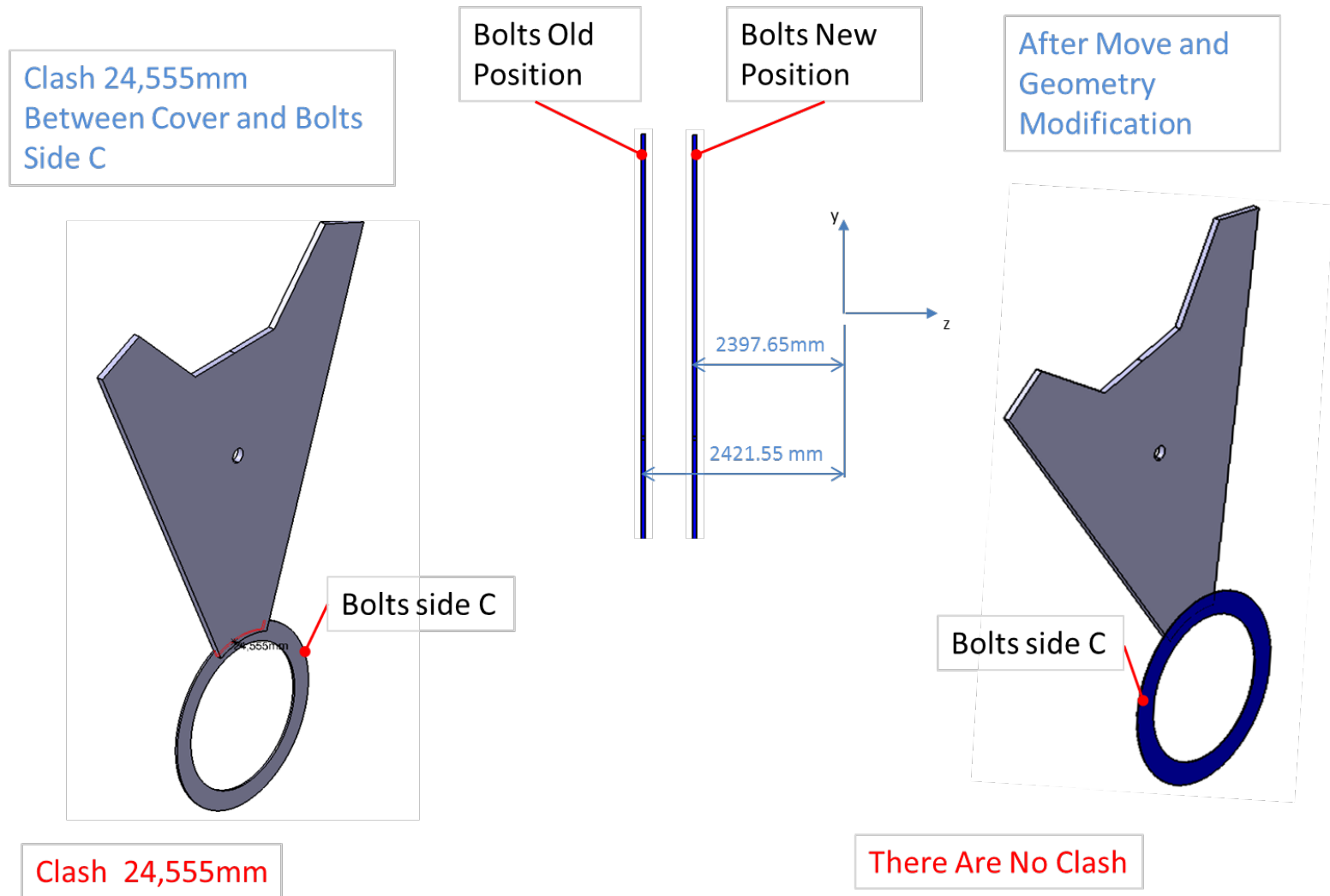
ATLAS End-CAP Toroid Study / Conflicts Checking

Internal Conflicts of ECT



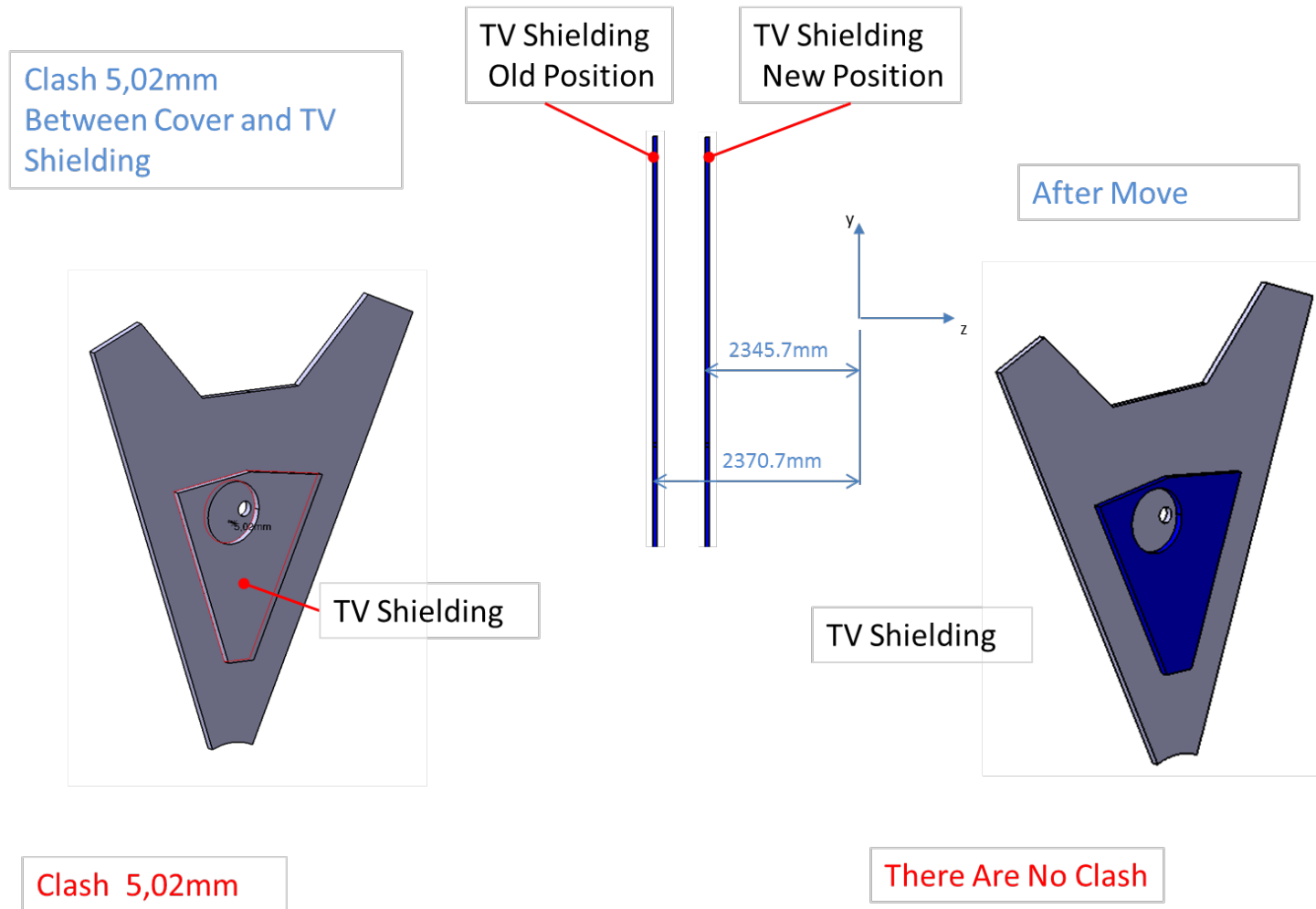
ATLAS End-CAP Toroid Study / Conflicts Checking

Internal Conflicts of ECT



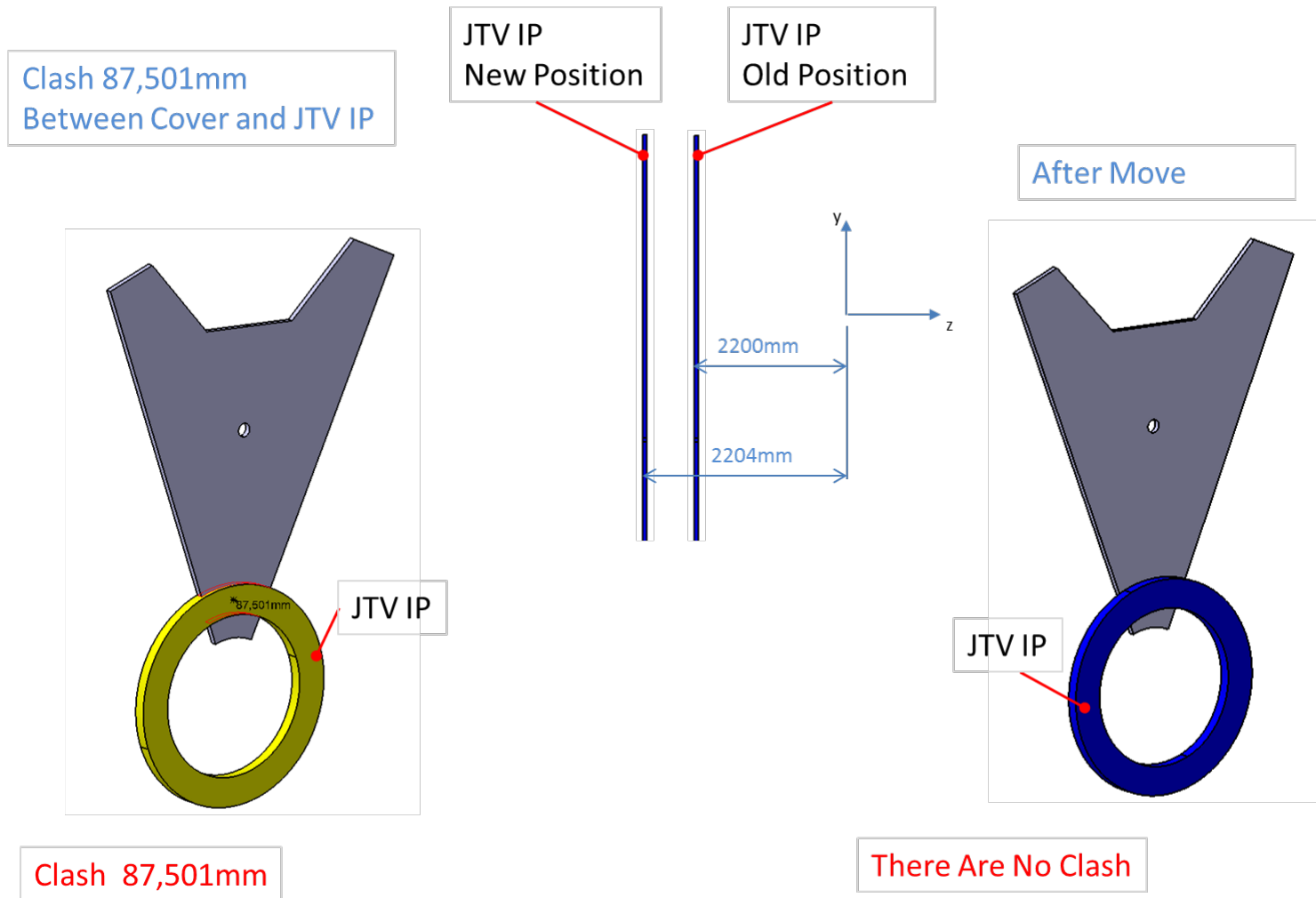
ATLAS End-CAP Toroid Study / Conflicts Checking

Internal Conflicts of ECT



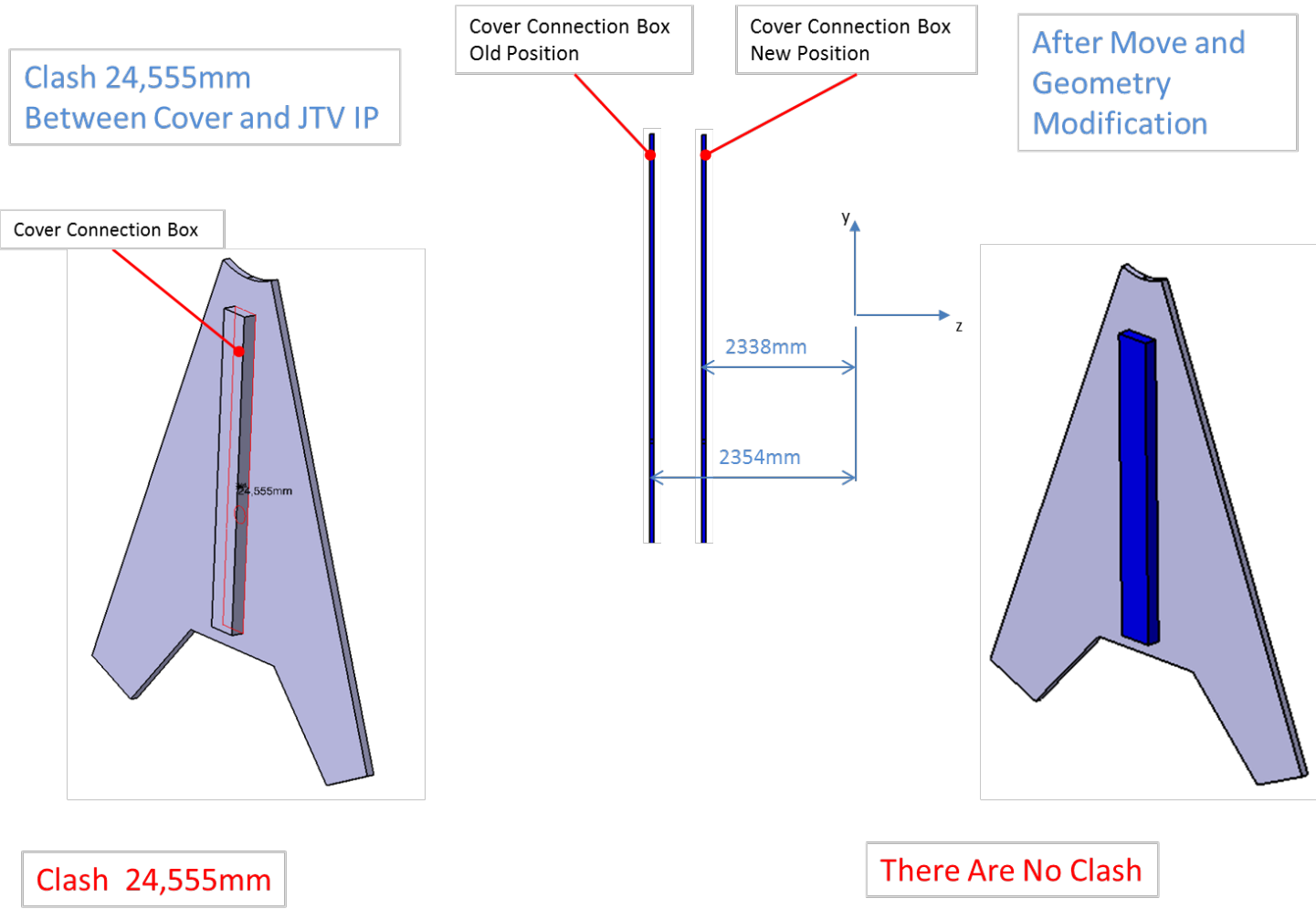
ATLAS End-CAP Toroid Study / Conflicts Checking

Internal Conflicts of ECT



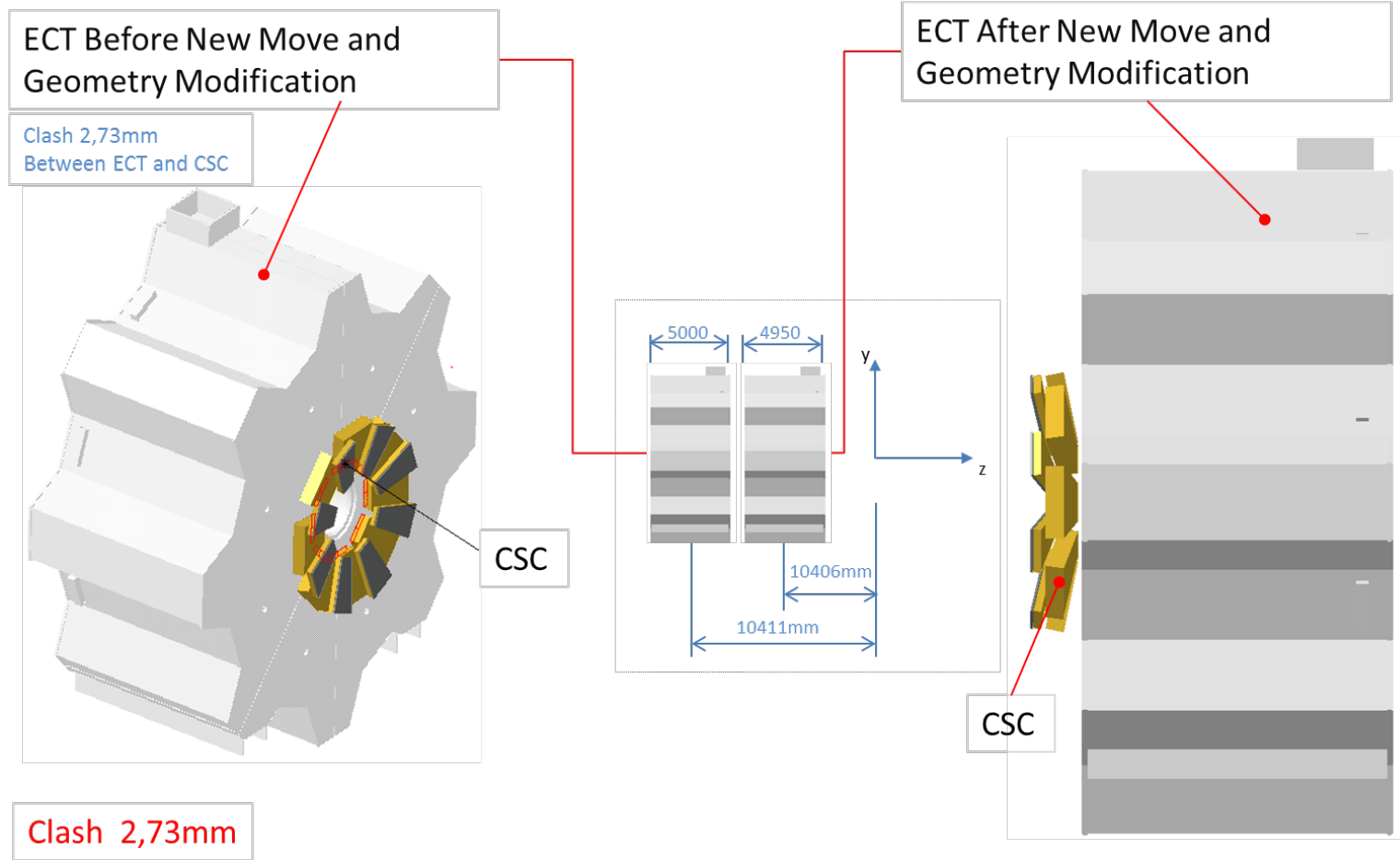
ATLAS End-CAP Toroid Study / Conflicts Checking

Internal Conflicts of ECT



ATLAS End-CAP Toroid Study / Conflicts Checking

External Conflicts of ECT

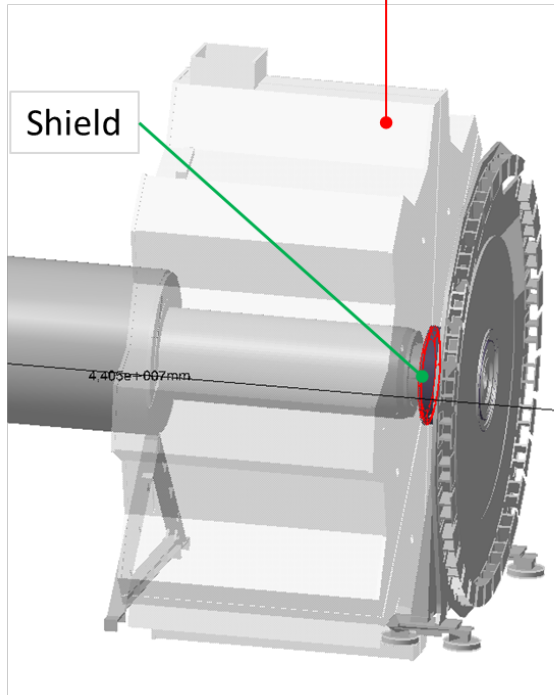


ATLAS End-CAP Toroid Study / Conflicts Checking

External Conflicts of ECT

ECT Before New Move and Geometry Modification

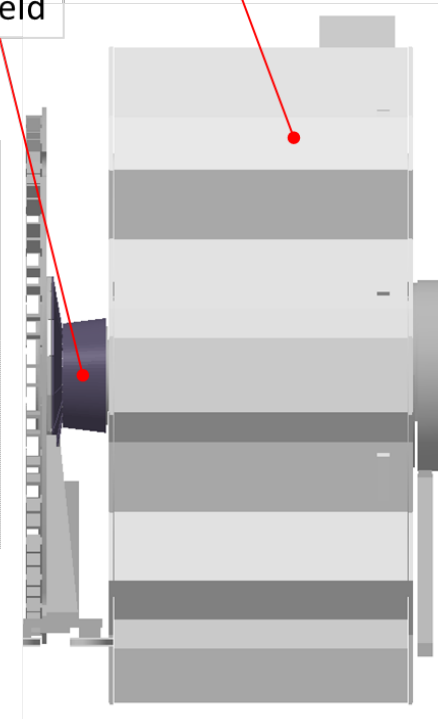
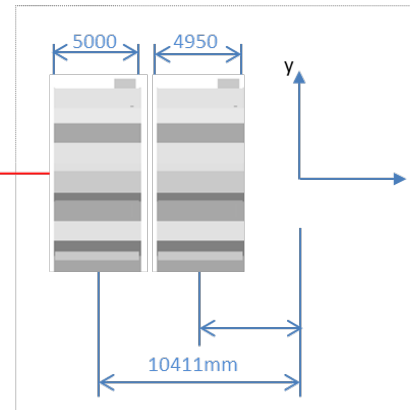
Clash 2,73mm
Between ECT and Shield



Clash 4,4mm

ECT After New Move and Geometry Modification

Shield



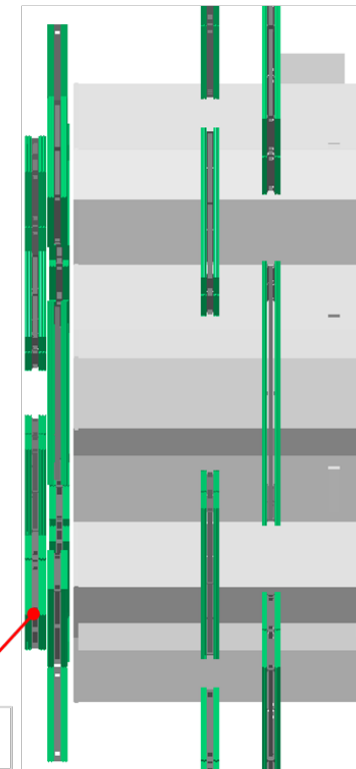
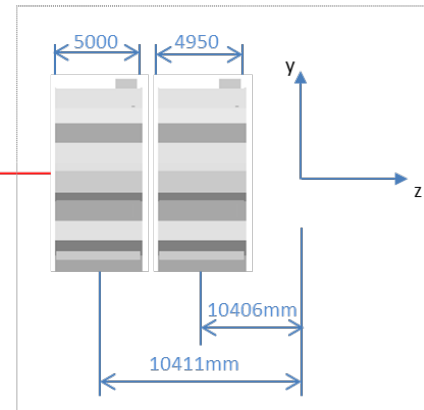
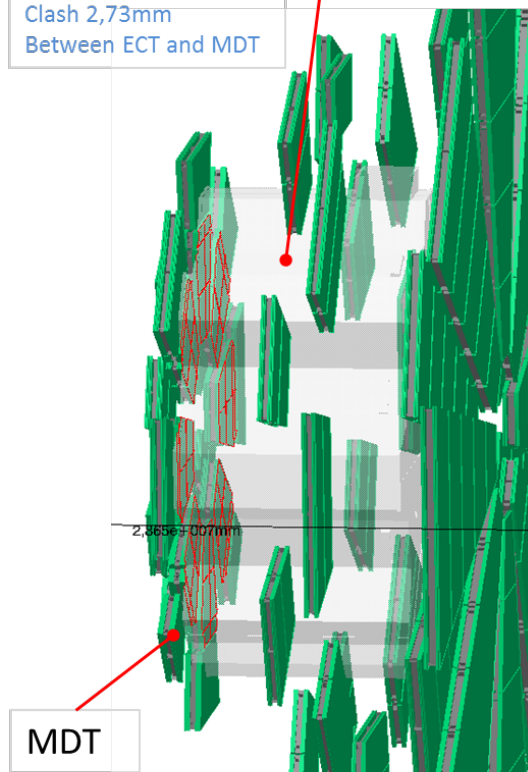
There Are No Integration Conflicts

ATLAS End-CAP Toroid Study / Conflicts Checking

External Conflicts of ECT

ECT Before New Move and Geometry Modification

Clash 2,73mm
Between ECT and MDT



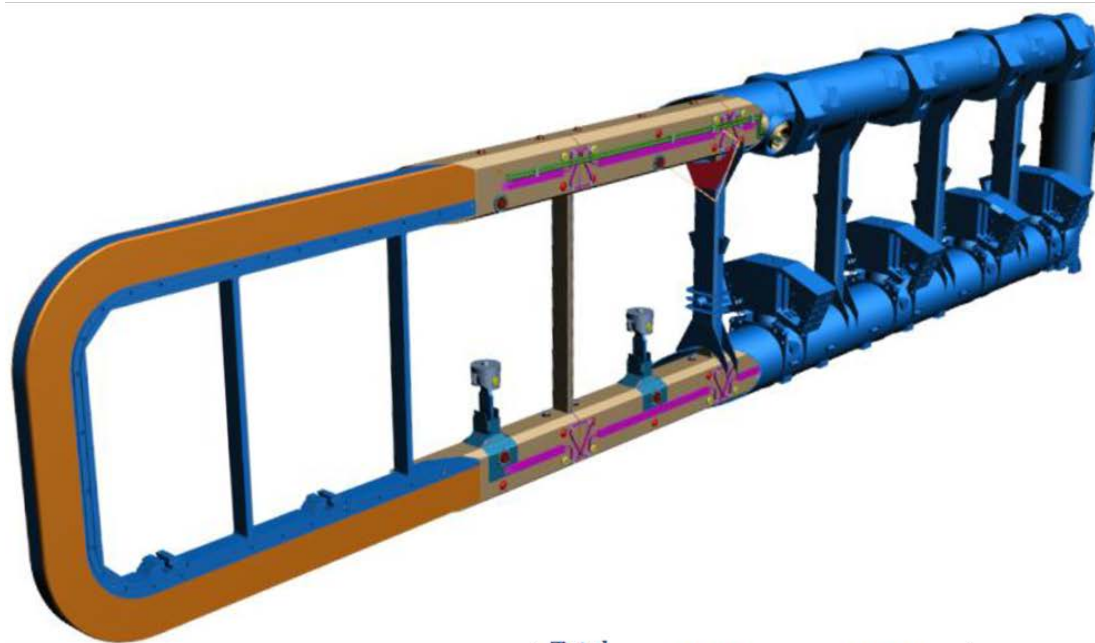
Clash 2,86mm

Conclusions of End-CAP Toroid Study

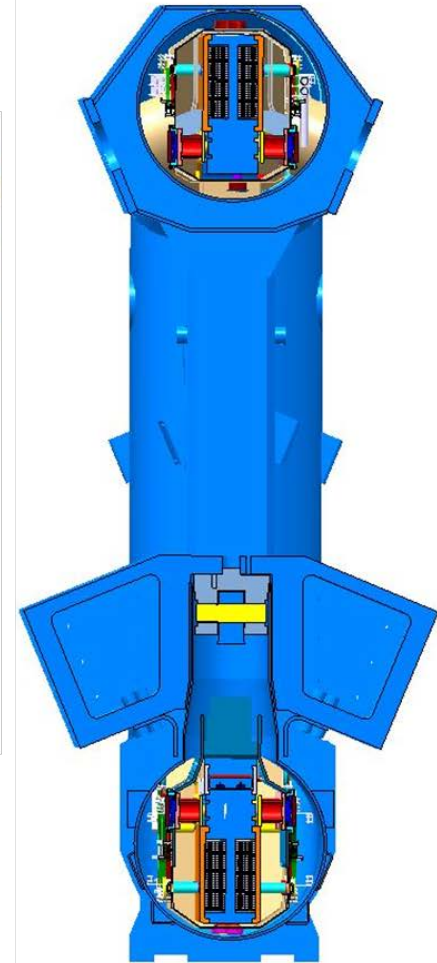
1. Compare analyse of CATIA vs XML shows >20% difference in volume and weight for majority of components
2. The grouping of volumes in the two geometry systems may differ somewhat, but the distribution of mass in the detector still shows significant differences
3. Most big discrepancies were detected for BoreTube assembly – 3 tonnes; TieRod assembly – 2 tonnes and Turret assembly – 960 kg
4. Conflicts analyses discover substantial integration conflicts for internal assembly of ECT as well external conflicts with surrounded components of detector

ATLAS Coil Study

- ATLAS detector have 8 identical Coils



Total	24.75	92348
	Volume (m ³)	Weight (kg)

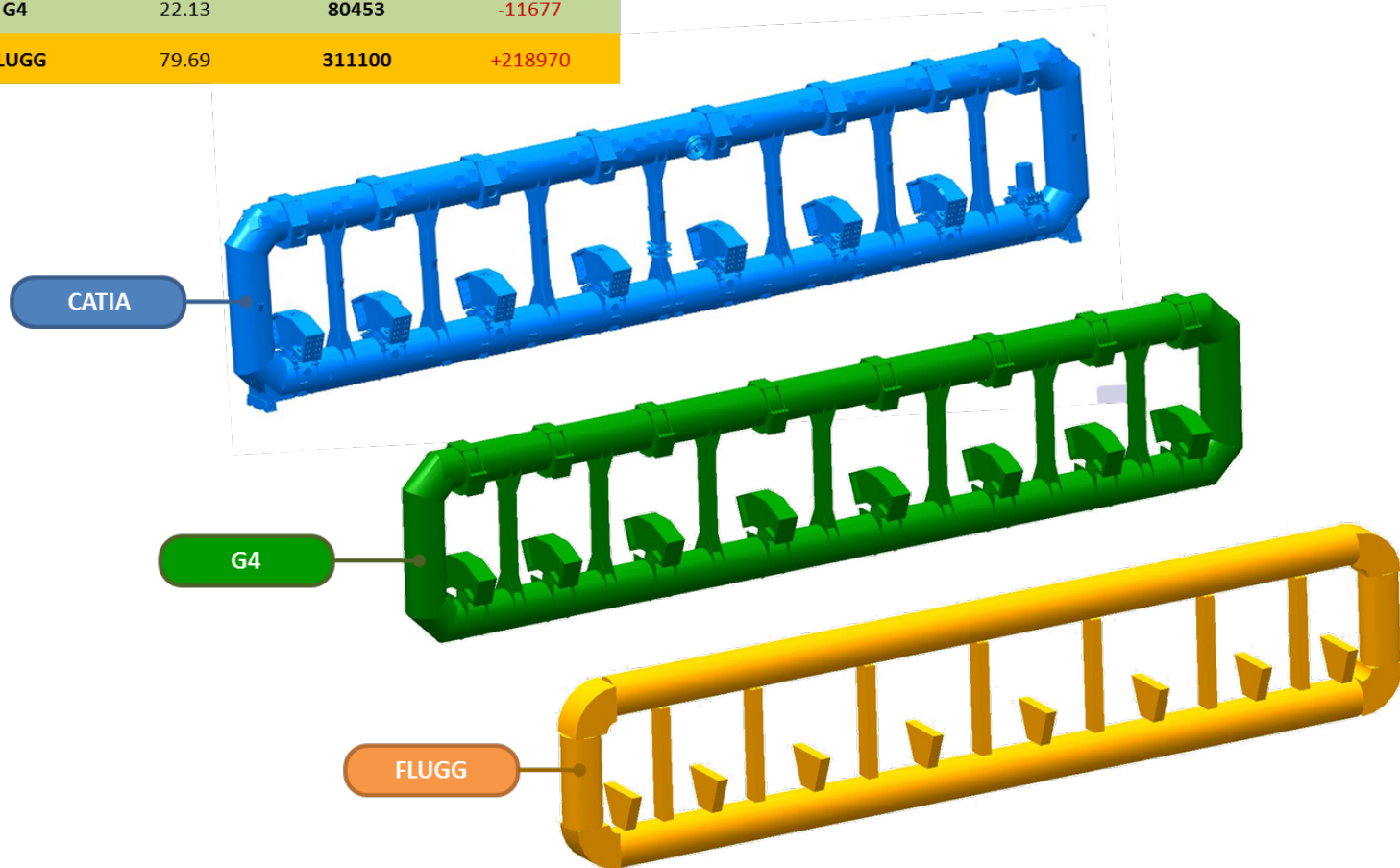


- Source geometry has been taken from SmarTeam Engineering Database:
 - Path : ATLAS2009/Detector System/Magnets ATLAS/Toroid Magnets ATLAS/Barrel Toroid Magnet ATLAS/TB coils
 - Model: **ST0301587 TB COIL SEC2 (id: CAD000323373)**
 - Date : 01/11/2011
- 225 manufacturing drawings have been founded on CDD and missing parts was added to primary Smarteam geometry

ATLAS Coil Study

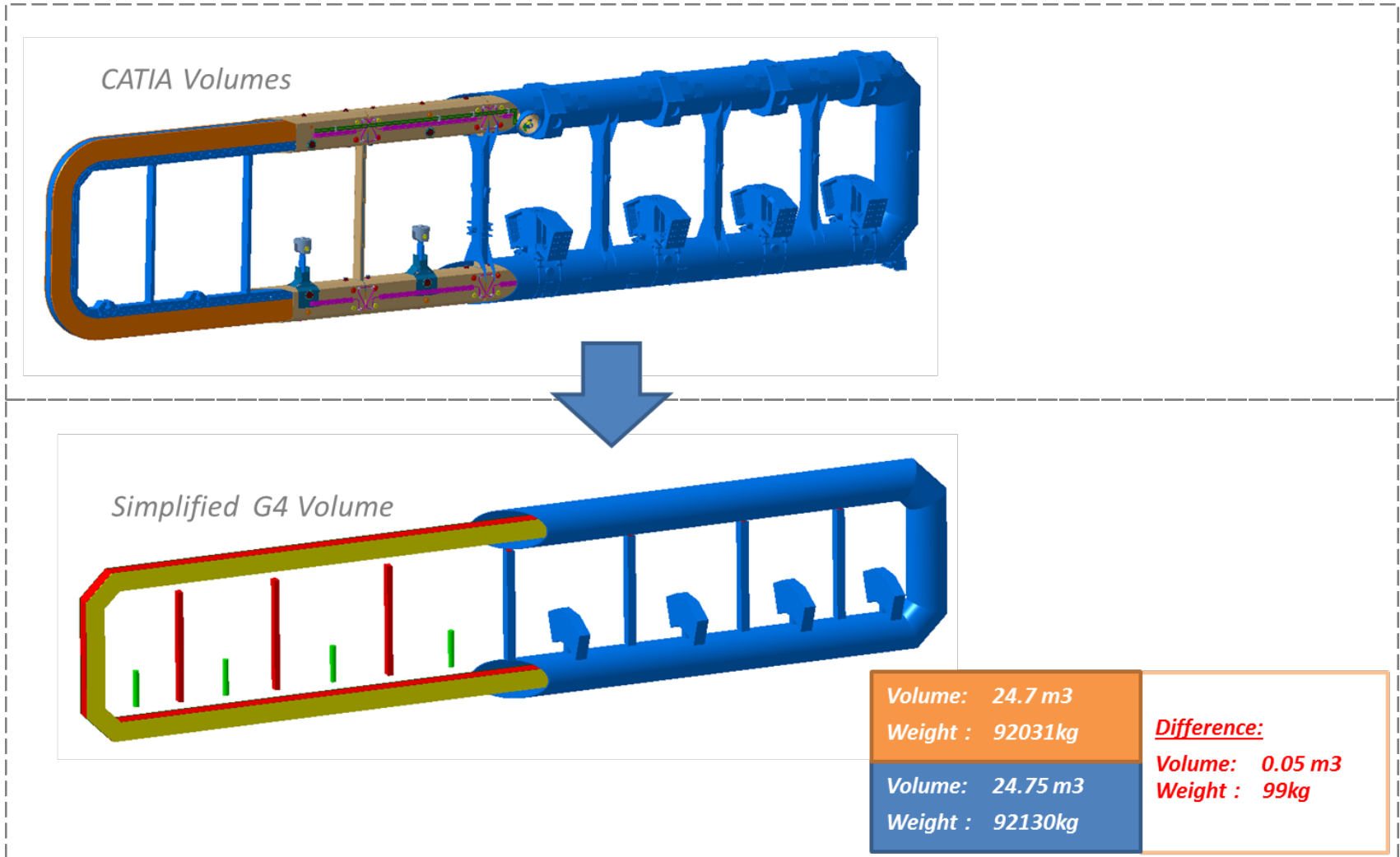
■ Compare Analyses

Model	Volume (m3)	Weight (kg)	Difference (kg)
CATIA	24.75	92130	
G4	22.13	80453	-11677
FLUGG	79.69	311100	+218970



ATLAS Coil Study

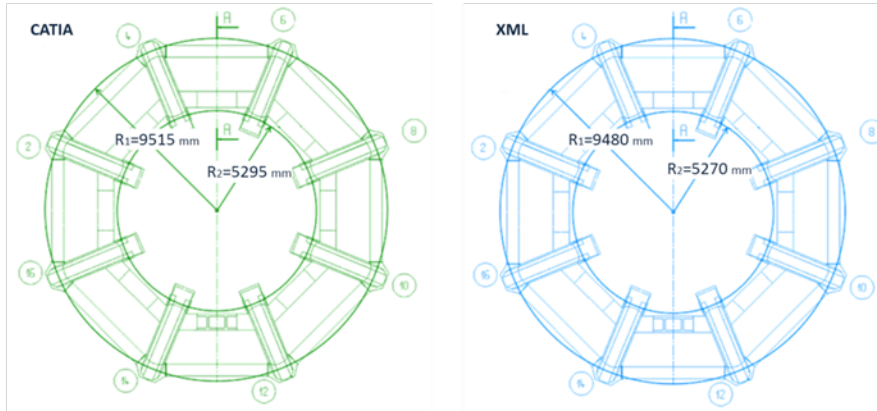
- Simplification of Assembly



ATLAS Coil Study

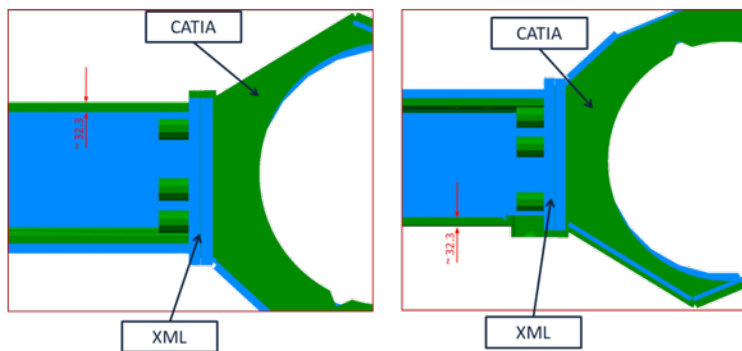
Integration Conflicts Analyses

COIL's + Warm Structure Displacement

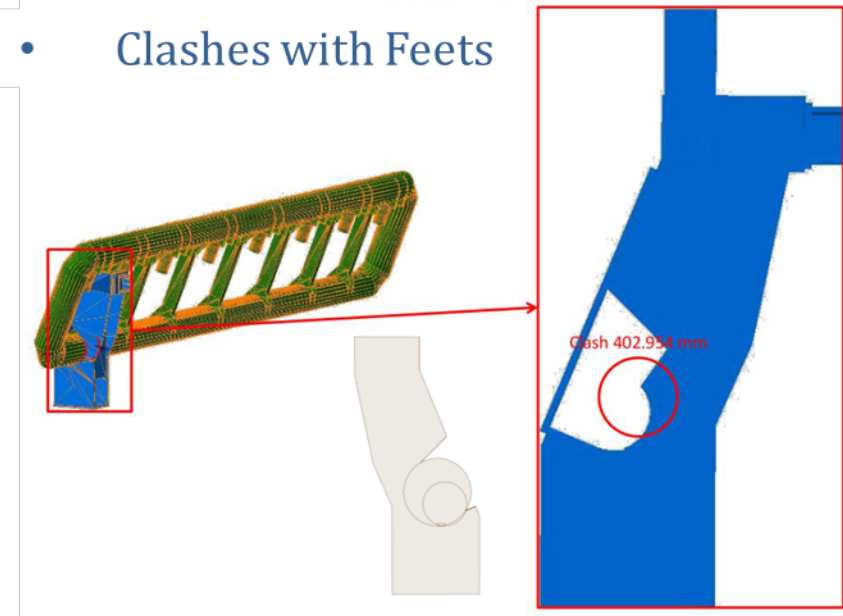


$$\Delta_{R_1} = R1|_{\text{CATIA}} - R1|_{\text{XML}} = 9515 \text{ mm} - 9480 \text{ mm} = 35 \text{ mm}$$
$$\Delta_{R_2} = R2|_{\text{CATIA}} - R2|_{\text{XML}} = 5295 \text{ mm} - 5270 \text{ mm} = 25 \text{ mm}$$

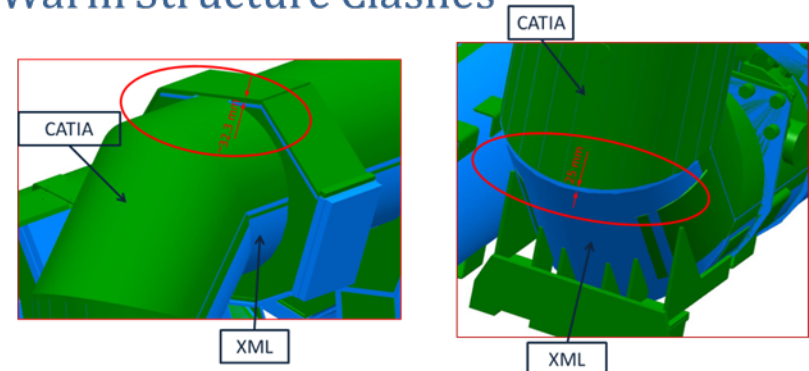
Warm Structure Clashes



Clashes with Feets



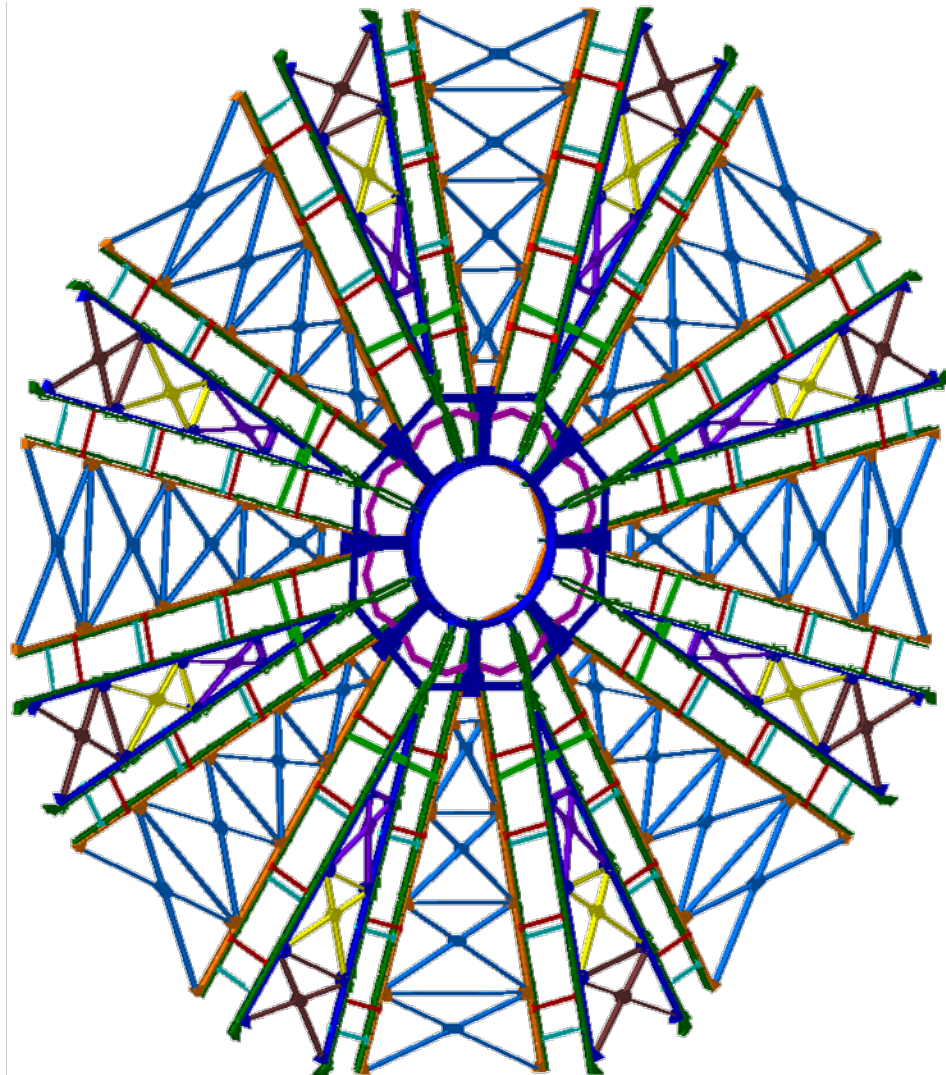
Warm Structure Clashes



Conclusions of Coil Study

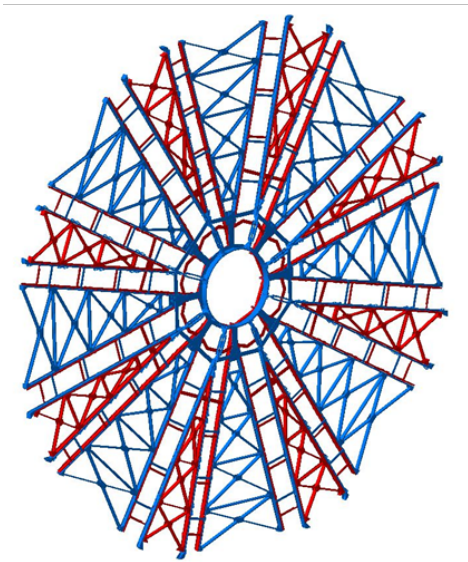
1. Compare analyse shows big differences in volume and weight between CATIA and XML descriptions
2. 11.6 tonnes missed materials were discovered for GEANT-4 geometry descriptions
3. 219 tonnes added materials were discovered for FLUGG geometry descriptions
4. Conflicts analyses discover substantial integration conflicts for internal assembly of Coil as well external conflicts with feet's of detector.
5. 35mm dispositioning of Coil has been discovered

MDT Supports Study



MDT Supports Study

■ Calculation of Total Volume and Weight



Big Sector Wheel

$$\begin{aligned}
 5'822 \text{ kg} \text{ | Total Weight} &= 1419\text{kgs} \text{ | Vol.1} & + 918\text{kgs} \text{ | Vol.2} & + 339\text{kgs} \text{ | Vol.3} + \\
 &+ 773.5\text{kgs} \text{ | Vol.4,1,4,2} & + 708.5\text{kgs} \text{ | Vol.5} & + 1216\text{kgs} \text{ | Vol.6,1-6.8} \\
 &+ 448\text{kgs} \text{ | Bolts\&Nuts} & &
 \end{aligned}$$

$$\begin{aligned}
 2.0464 \text{ m}^3 \text{ | Total Volume} &= 0.0657 \text{ m}^3 \text{ | Vol.1} & + 0.0425 \text{ m}^3 \text{ | Vol.2} & + 0.0157 \text{ m}^3 \text{ | Vol.3} \\
 &+ 0.0358 \text{ m}^3 \text{ | Vol.4,1,4,2} & + 0.0328 \text{ m}^3 \text{ | Vol.5} & + 0.0563 \text{ m}^3 \text{ | Vol.6,1-6.8} \\
 &+ 0.056 \text{ m}^3 \text{ | Bolts\&Nuts} & &
 \end{aligned}$$

Small Sector Wheel

$$\begin{aligned}
 4'710 \text{ kg} \text{ | Total Weight} &= 1438.56 \text{ kgs} \text{ | Vol.1} & + 1051.92 \text{ kgs} \text{ | Vol.2} & + 397.44 \text{ kgs} \text{ | Vol.3} \\
 &+ 306.72 \text{ kgs} \text{ | Vol.4} & + 248.4 \text{ kgs} \text{ | Vol.5} & + 216 \text{ kgs} \text{ | Vol.6} \\
 &+ 239.76 \text{ kgs} \text{ | Vol.7} & + 162 \text{ kgs} \text{ | Vol.8} & + 125.28 \text{ kgs} \text{ | Vol.9} \\
 &+ 524 \text{ kgs} \text{ | Bolts\&Nuts} & &
 \end{aligned}$$

$$\begin{aligned}
 1.6159 \text{ m}^3 \text{ | Total Volume} &= 0.5328 \text{ m}^3 \text{ | Vol.1} & + 0.3896 \text{ m}^3 \text{ | Vol.2} & + 0.1472 \text{ m}^3 \text{ | Vol.3} \\
 &+ 0.1136 \text{ m}^3 \text{ | Vol.4} & + 0.092 \text{ m}^3 \text{ | Vol.5} & + 0.08 \text{ m}^3 \text{ | Vol.6} \\
 &+ 0.0888 \text{ m}^3 \text{ | Vol.7} & + 0.06 \text{ m}^3 \text{ | Vol.8} & + 0.0464 \text{ m}^3 \text{ | Vol.9} \\
 &+ 0.0655 \text{ m}^3 \text{ | Bolts\&Nuts} & &
 \end{aligned}$$

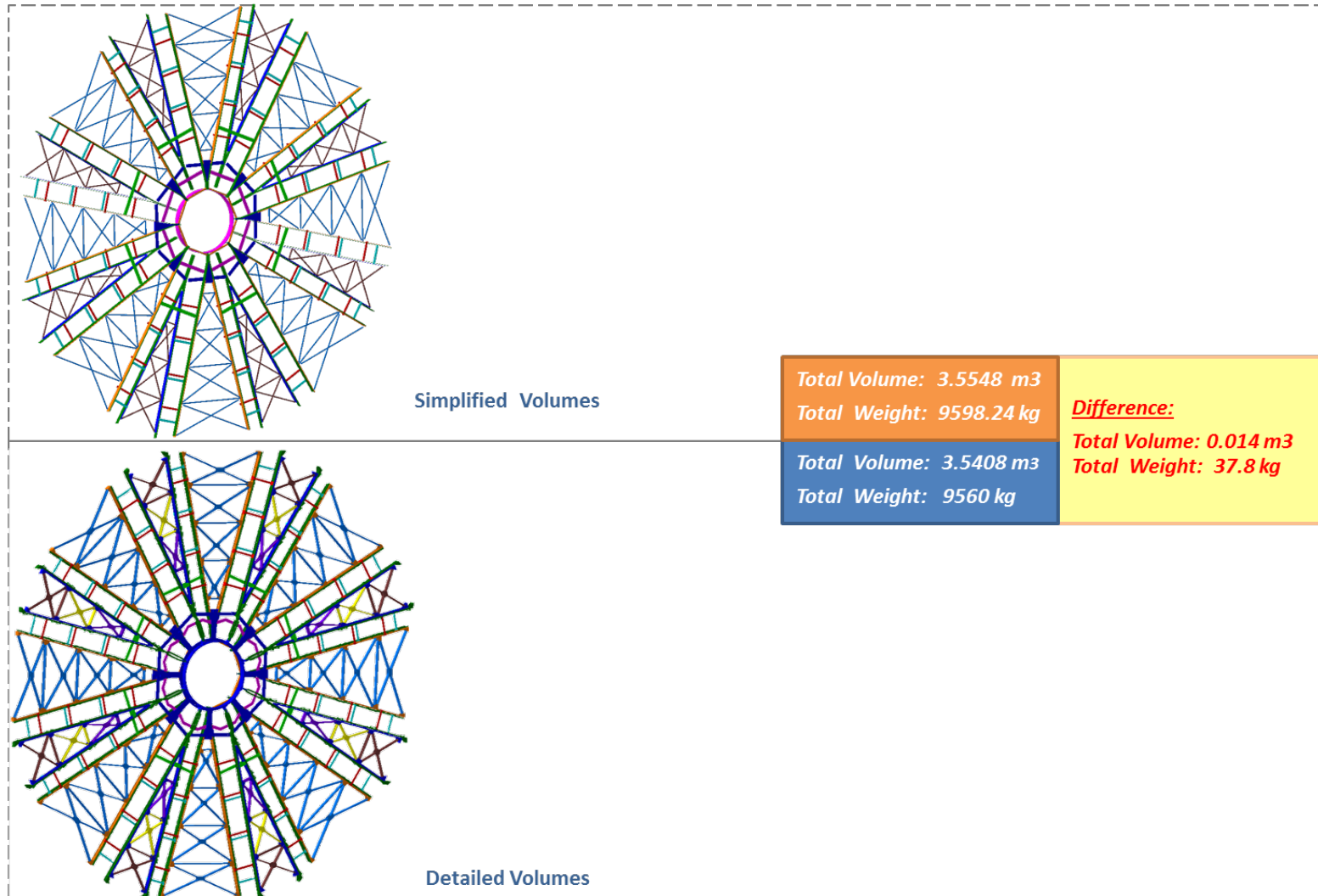
BW MDT All Sector Total

3.6723
Volume (m³)

10'532
Weight (kgs)

MDT Supports Study

■ Simplification of Large and Small Sectors

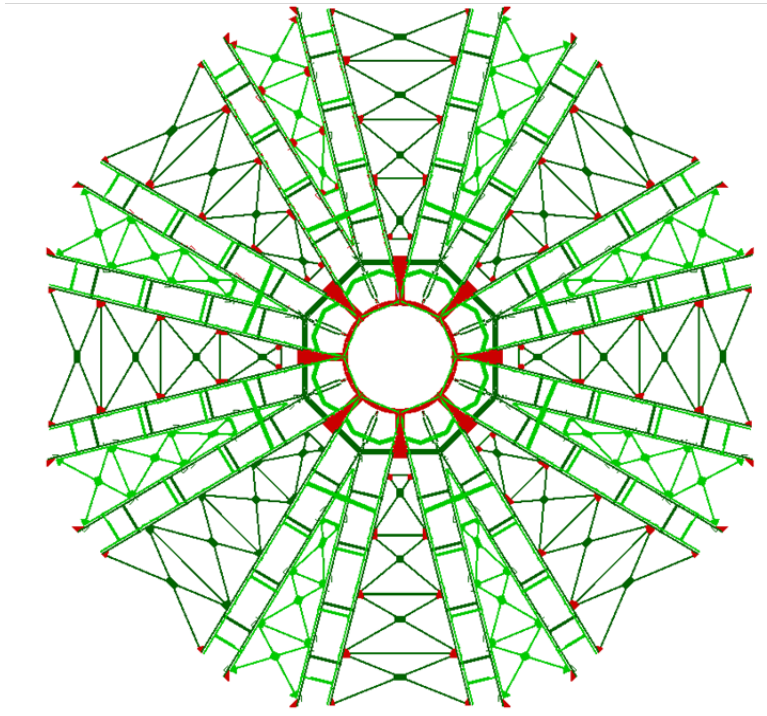


MDT Supports Study

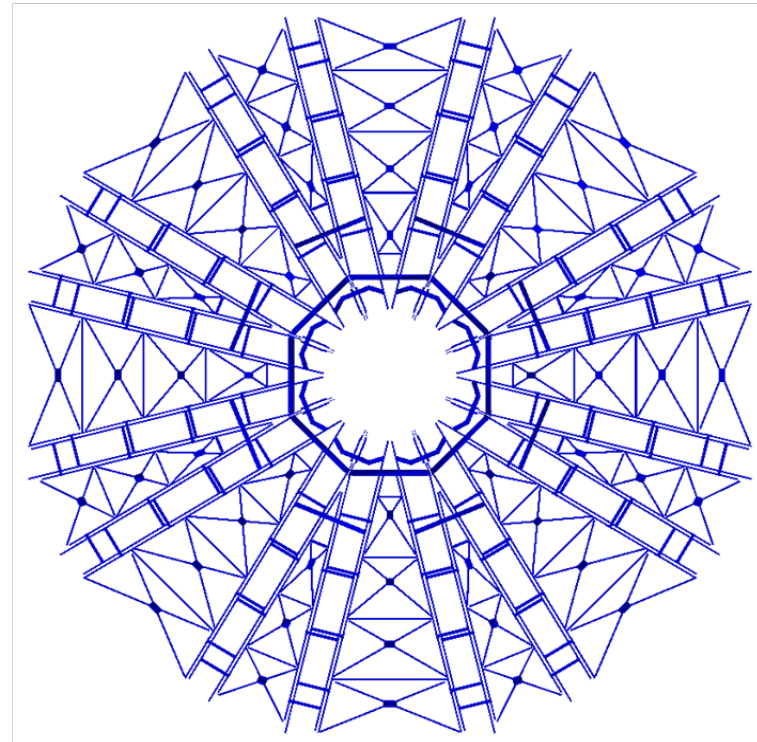
■ Integration Conflicts Analyses

Model	Material	Density (kg/m ³)	Volume (m ³)	Weight (kgs)	Missing (kgs)
CATIA	Aluminum/Stainless Steel	2700 / 8000	3.6723	10'532	
PERSINT/XML	Aluminum	2700	2.3184	6'260	-4'272

CATIA Model

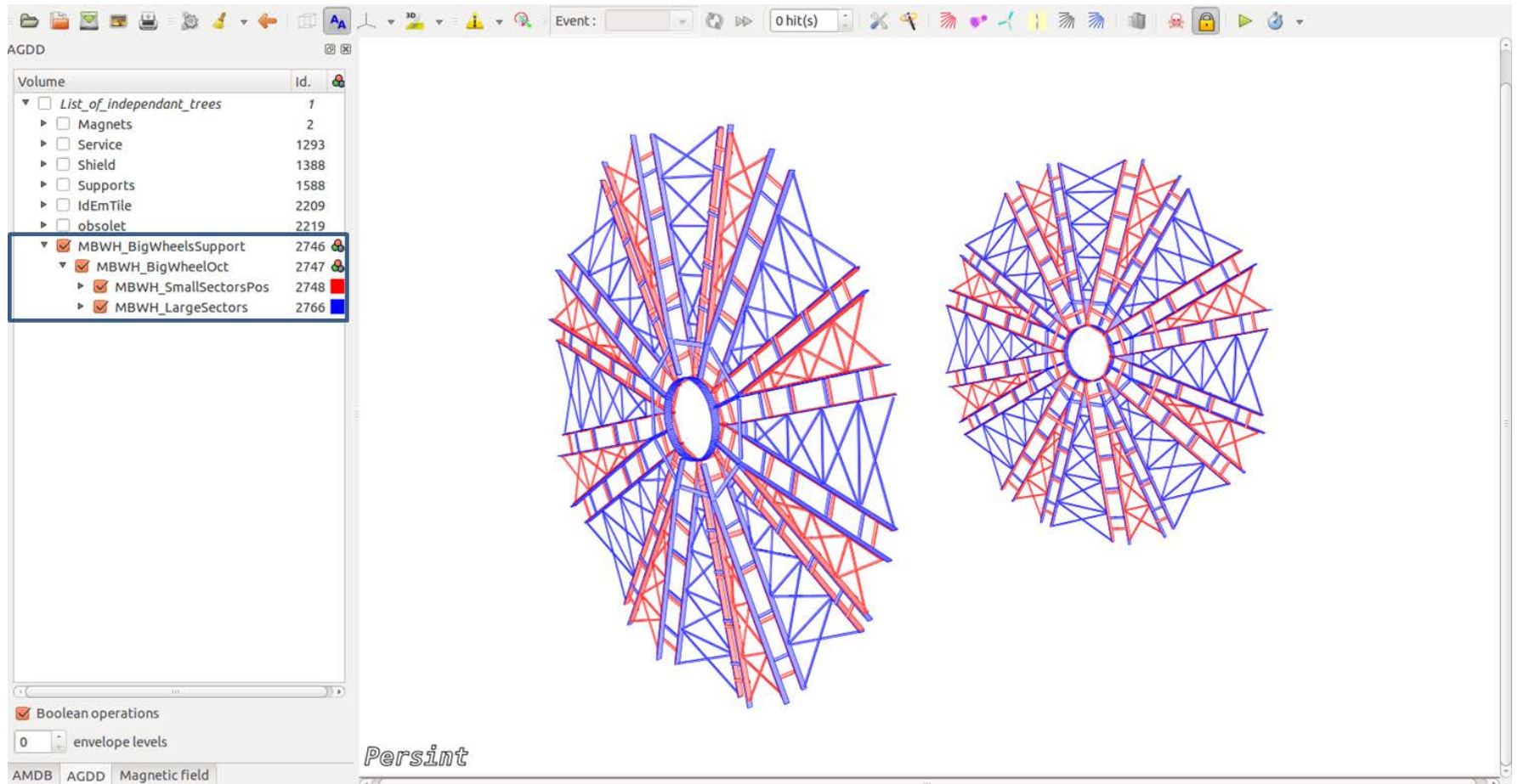


GEANT-4 Model



MDT Supports Study

■ Integration Conflicts Analyses



No Integration Conflicts

Conclusions of MDT Support Study

1. Compare analyse shows big differences in volume and weight between CATIA and XML descriptions
2. 4.2 tonnes missed materials were discovered for GEANT-4 geometry descriptions
3. There are no Integration Conflicts

Final Conclusions

General Conclusions

- Hypothesis #01 has been approved: Simulation software infrastructure added geometry inaccuracies
 1. For all type of detector geometries dimensional, form and positioning faults are caused by *Boolean* operations
 2. All internal surfaces received by *Boolean* subtraction of parametrical primitives from *Box* brings 0 faults
 3. *Boolean* operation correlated with *Move/Rotation* transactions in GEANT. Once *Boolean* operation is implemented transactions generating geometry displacements of support points of geometry created by *Boolean* procedures
 4. For all external surfaces created by subtraction of parametrical primitives from *Box*, *Boolean* operation don't correlated with *Move/Rotation* transactions

General Conclusions

5. For some internal surfaces created by subtraction of parametrical primitives from *Polygon* methods, *Boolean* operation don't correlated with *Move* transactions
6. *Arbitrary Polygon* method is most reliable way to simulate detector geometry in simulation software infrastructure
7. *Boolean* operation cause clashes (~1.28mm) inside geometry which is "visible" for large size volumes and not visible for smaller because of limitations of CATIA tool using for analyses
8. Increasing of dimensional values of geometry are exponentially increase values of inaccuracies added by *Boolean* operations

General Conclusions

- Hypothesis #02 has been approved: Geometry descriptions in simulation are not consistent with as-built geometry descriptions. As a result it may cause discrepancies between real and simulated data.
1. Compare analyses of ECT, Coils and MDT Supports show inconsistency with as-built geometry in terms of volumes, weight, positioning and existence of integration conflicts
 2. Compare analyse of ECT shows >20% difference in volume and weight for majority of components
 3. ECT Conflicts analyses discover substantial integration conflicts for internal assembly and external conflicts with surrounded components of detector as well
 4. For Coil Assembly 11.6 tonnes missed materials were discovered for GEANT-4 and 219 tonnes added materials were discovered for FLUGG geometry descriptions

General Conclusions

5. Coil's Conflicts analyses discover substantial integration conflicts for internal assembly and external conflicts with feet's of detector as well
6. Coil's dispositioning on 35mm has been discovered
7. For MDT Supports 4.2 tonnes missed materials were discovered for GEANT-4 geometry descriptions

- Comments are welcome

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Thanks for your attention!